

**Localized viscous heating observed
in a two-dimensional
strongly coupled dusty plasma**

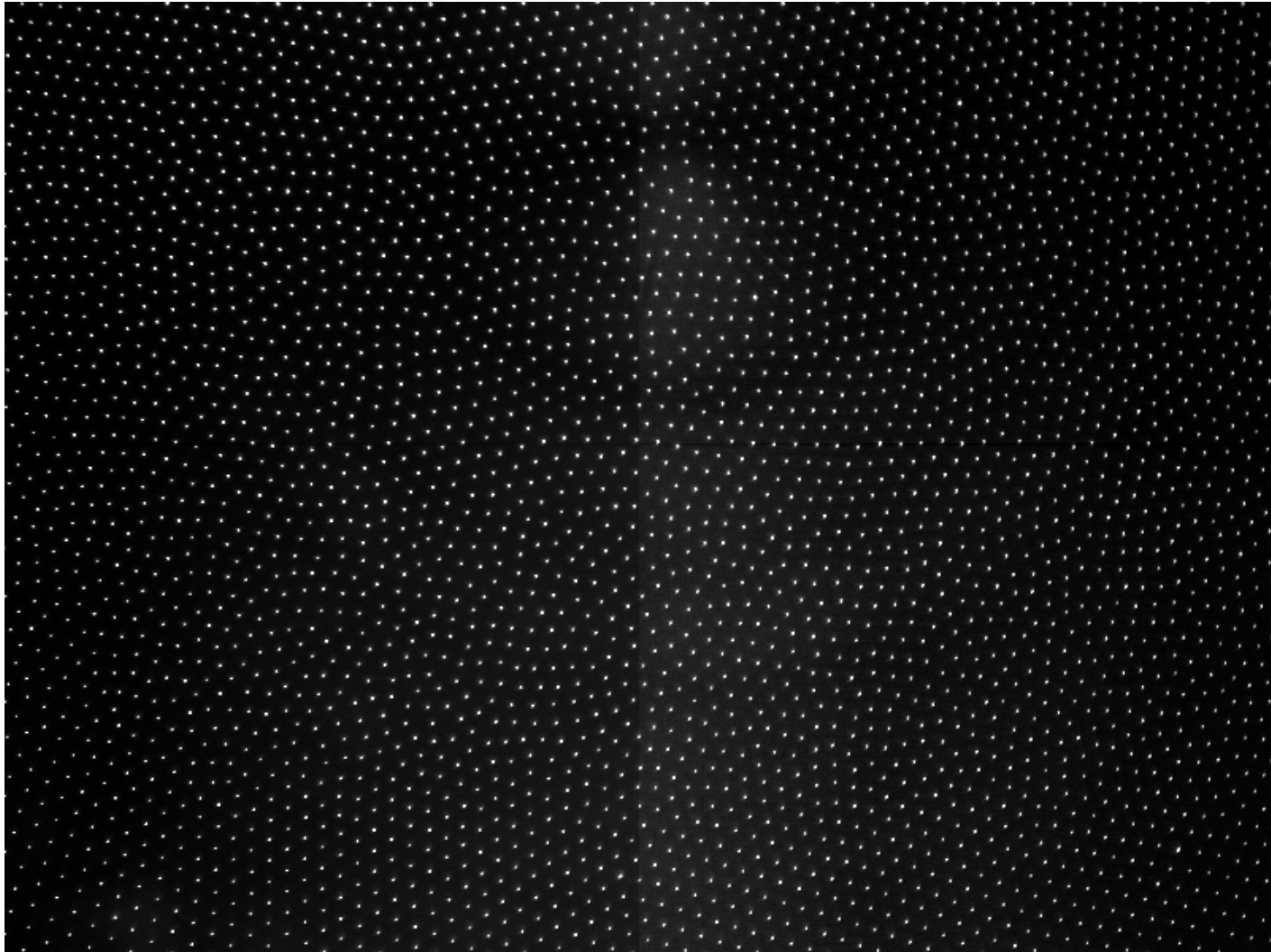


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Univ. of Iowa**

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Shear flow in 2D dusty plasma

Shear flow in dusty plasma



Fluids, in general

Transport coefficients

μ = viscosity

κ = thermal conductivity

These coefficients are material properties.

Viscous heating: it's where a lot of energy is lost

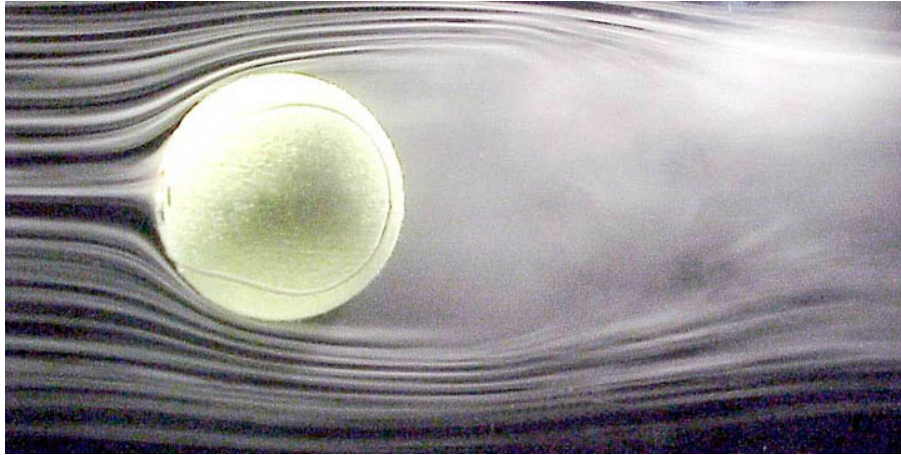


image: NASA

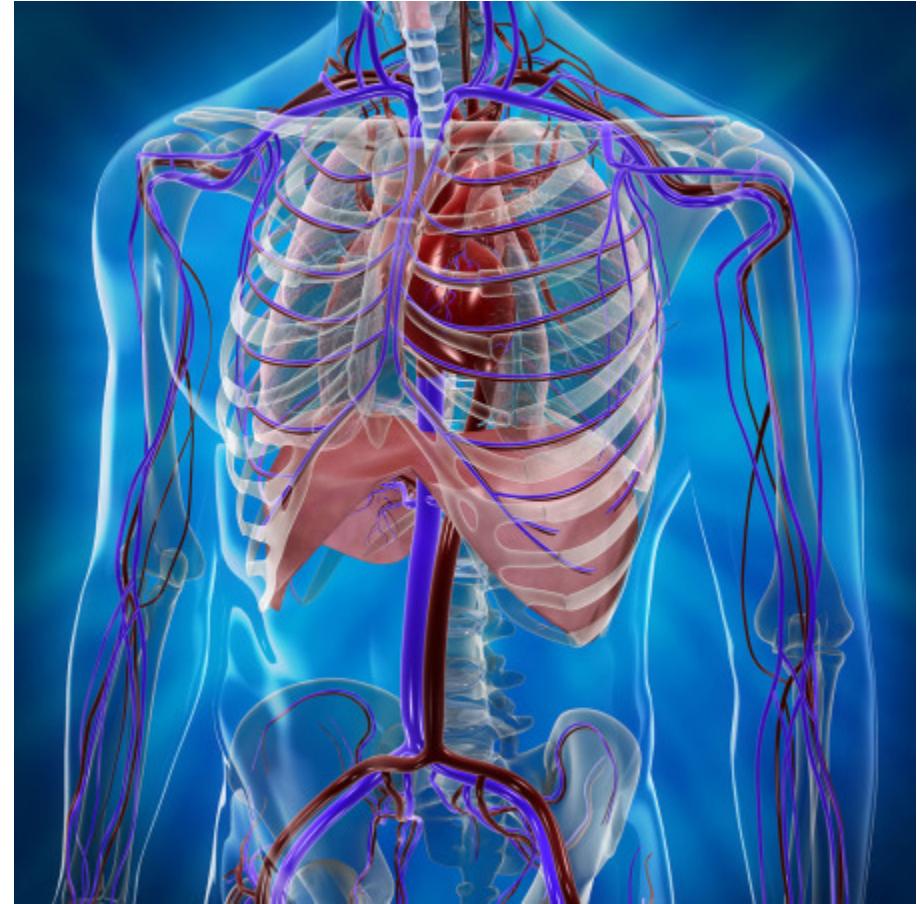
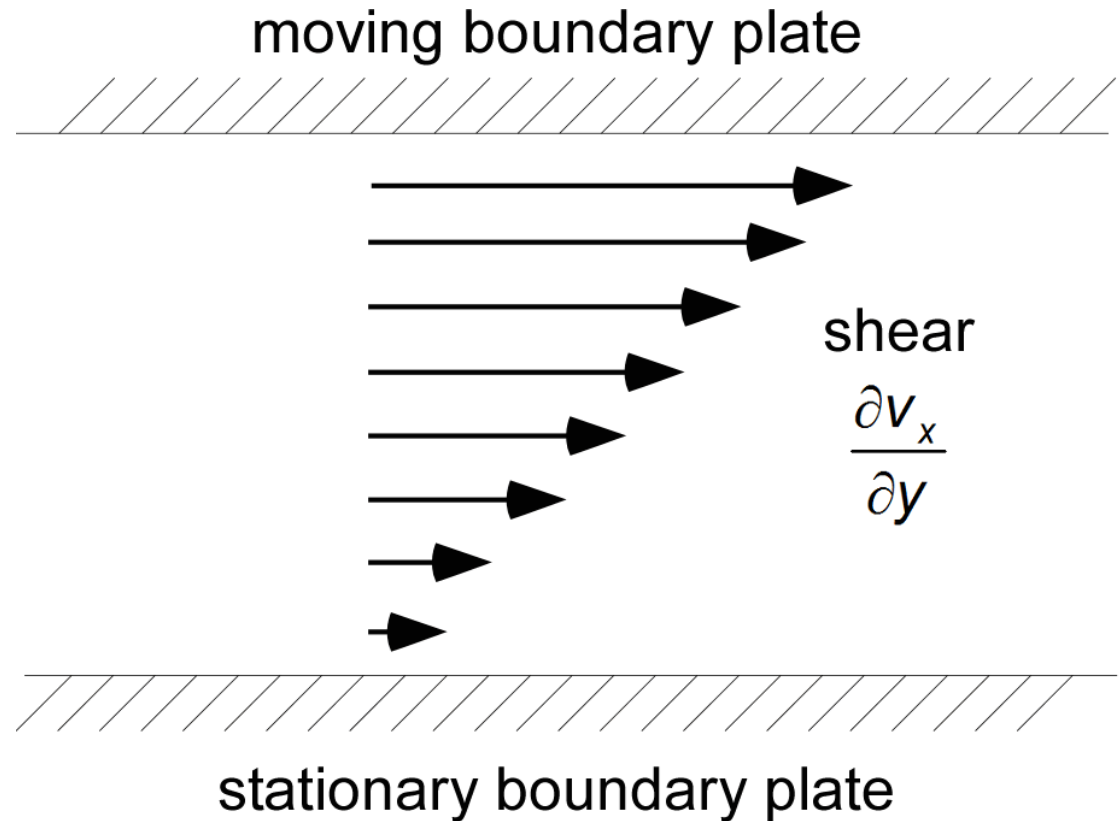


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Viscous heating happens in a sheared flow

Couette flow
between
two flat plates



Viscous heating happens in a sheared flow

“shear”

= transverse gradient of a flow velocity

$$= \partial v_x / \partial y$$

Heat generated $\propto (\partial v_x / \partial y)^2$

Hydrodynamic equations for Couette flow

momentum

$$\frac{\eta}{\rho} \nabla^2 \mathbf{v} = 0$$

energy

$$\frac{\kappa}{\rho} \nabla^2 T + \frac{\eta}{\rho} \left(\frac{\partial v_x}{\partial y} \right)^2 = 0$$

thermal
conduction 

 viscous
heating

μ = viscosity

κ = thermal conductivity

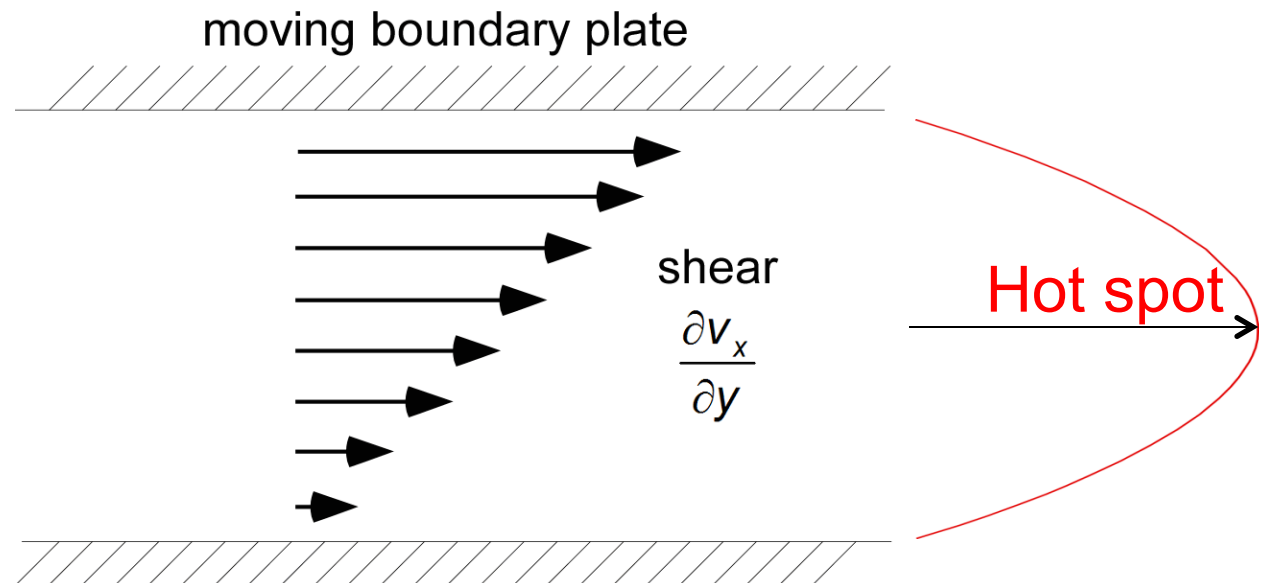
Solution of the hydrodynamic equations for Couette Flow

Solutions:

$$V_x \propto y$$

$$T \propto y^2 \text{ due to viscous heating}$$

$$T \propto \frac{\eta}{\kappa} \left(\frac{\partial V_x}{\partial y} \right)^2$$



viscous heating:

- should cause **hot-spots** in a flow
- but they aren't observed

Why aren't the hot spots observed?

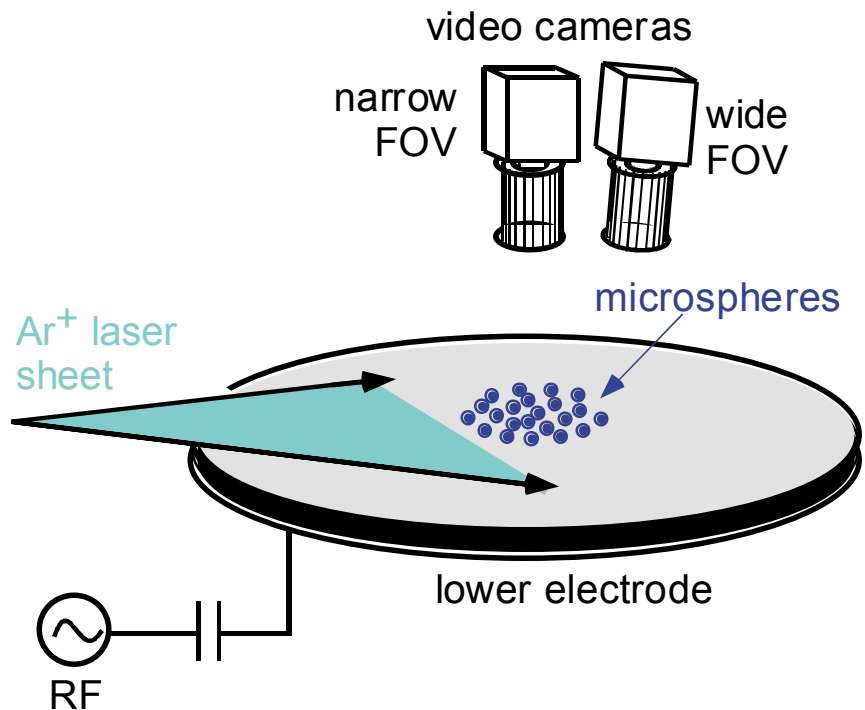
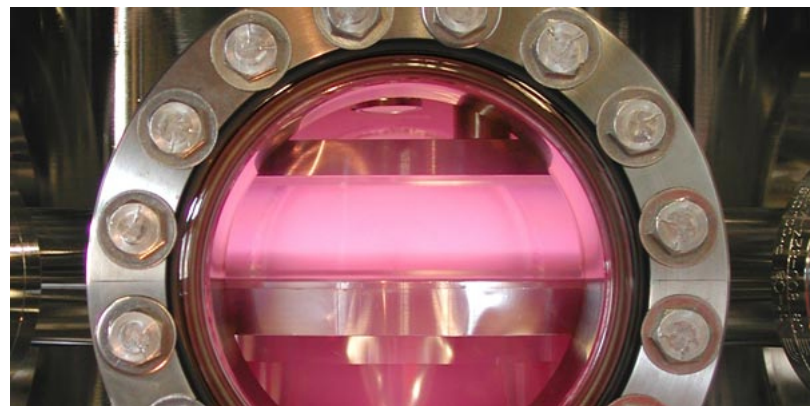
For most substances:

thermal conductivity κ is so large that $\nabla^2 T$ is tiny.

To observe a hot spot requires a combination of:

- Small κ thermal conductivity
- Large η viscosity
- Large $\partial v_x / \partial y$ shear
- Instrumentation for in-situ temp measurement

Experimental setup



Argon RF glow discharge:

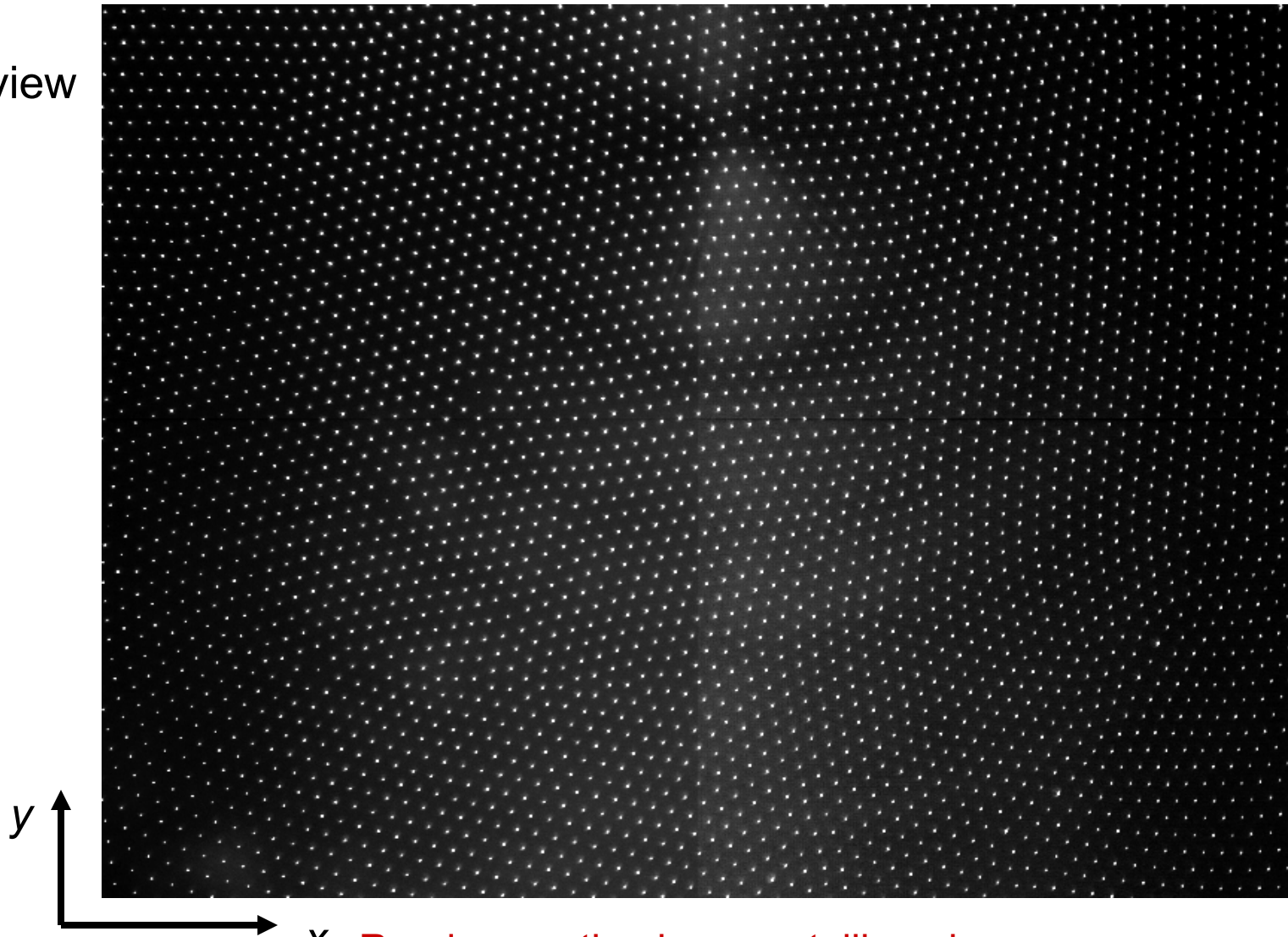
gas 15.5 mTorr Argon
RF low power, 13.6 MHz
 λ_D 0.53 mm

MF Polymer microspheres:

diameter 8.1 μm
number >11000 particles
interparticle dist. 0.50 mm
charge -9700 e

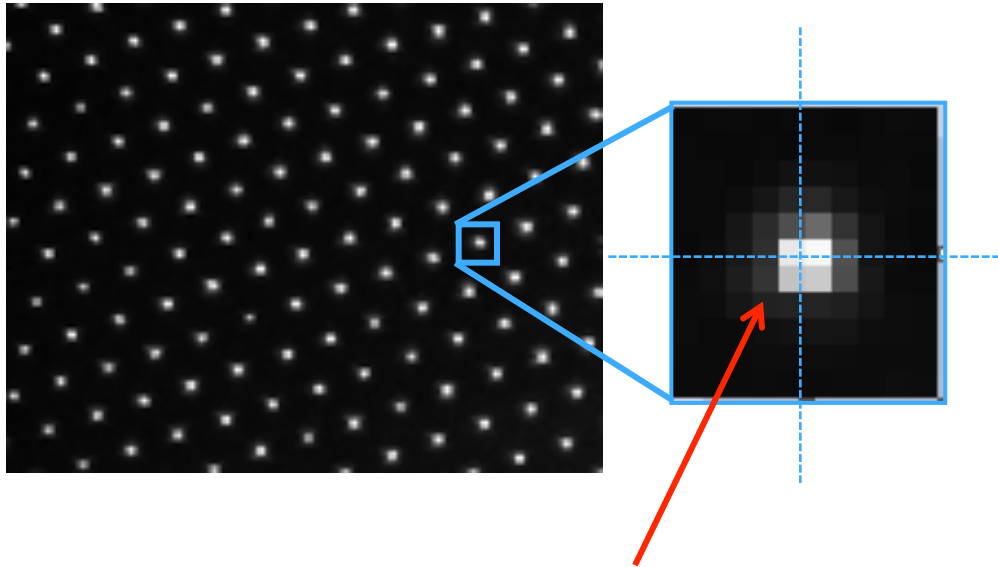
Narrow field of view

Top view



x Random motion in a crystalline phase

Measurements of particles



Intensity in pixel i is I_i

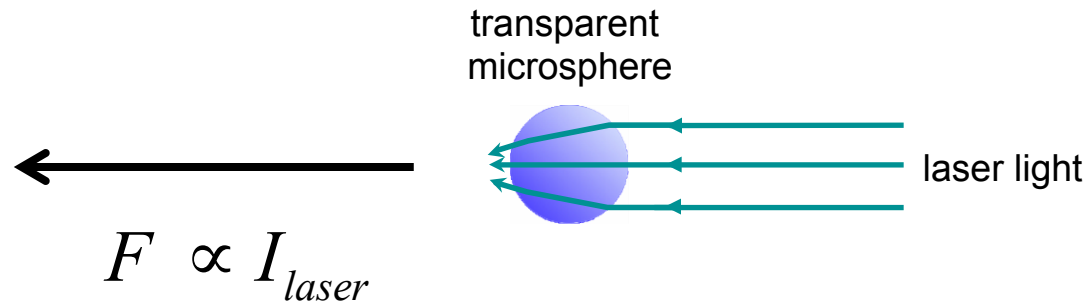
- Measure particle x, y positions

$$X = \frac{\sum (X_i I_i)}{\sum I_i}$$

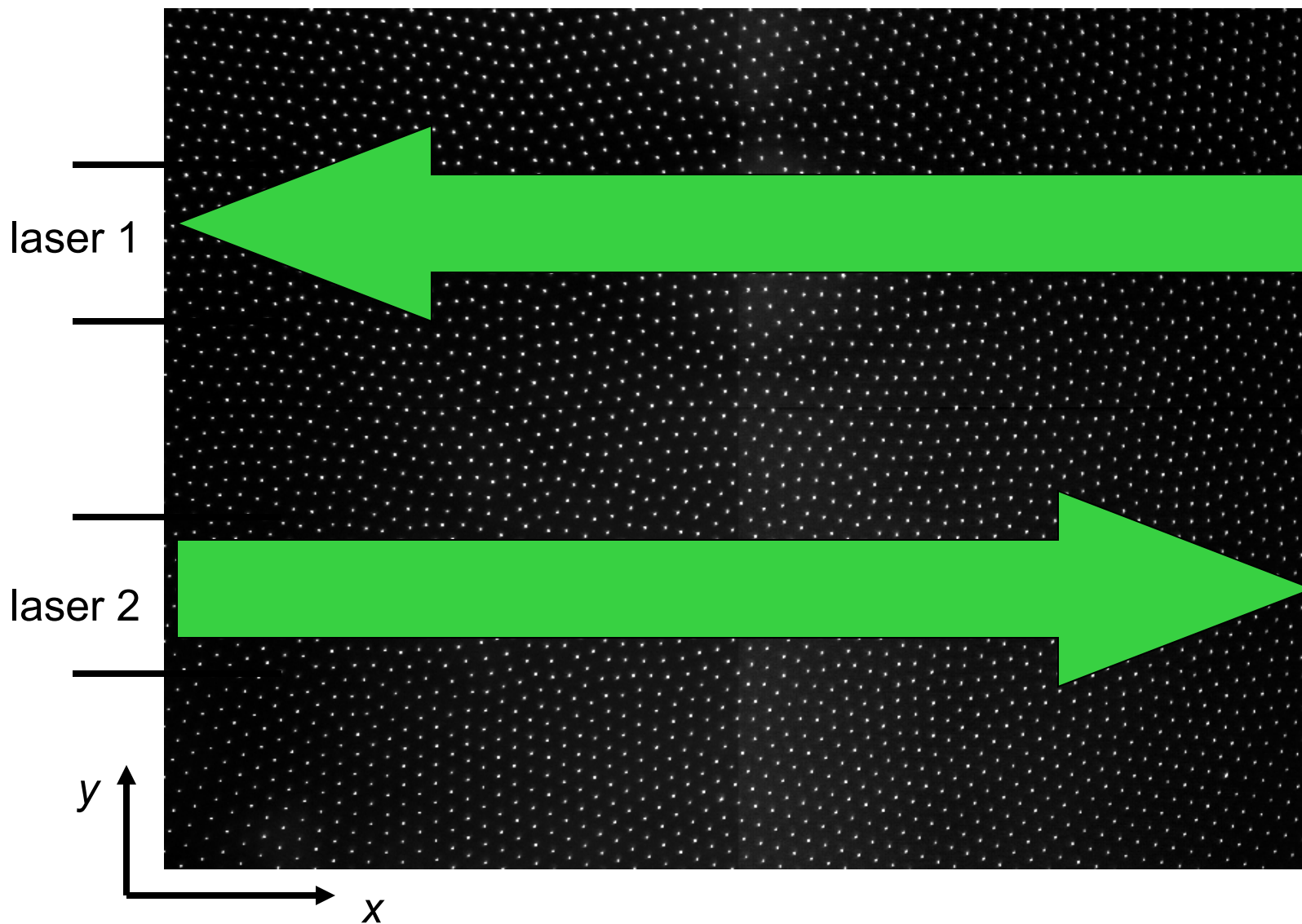
- Track particles from frame to frame

Yields time series for
positions & velocities of particles

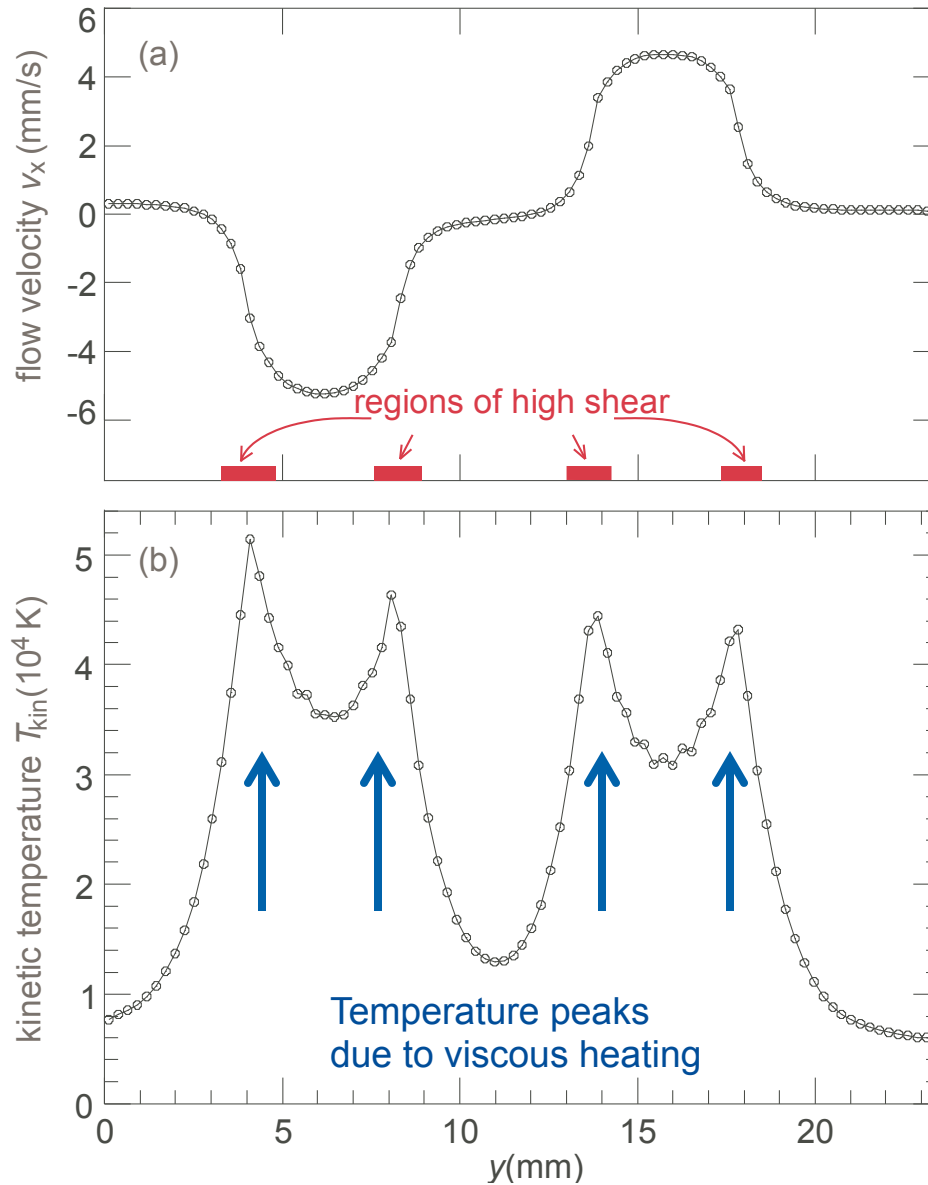
Manipulating particles using Radiation Pressure Force



Movie of the laser-driven shear flow



Results: profiles of flow velocity & temperature



flow velocity profile v_x

temperature profile T

Confirm the conclusion

To confirm that the peaks are due to viscous heating:

- Calculate the Brinkmann number

$$\text{Br} \equiv \frac{\eta \Delta v_x^2}{\kappa \Delta T}$$

- Confirm that it is of order unity



We require:

Δv_x

ΔT

} Flow parameters

η

κ

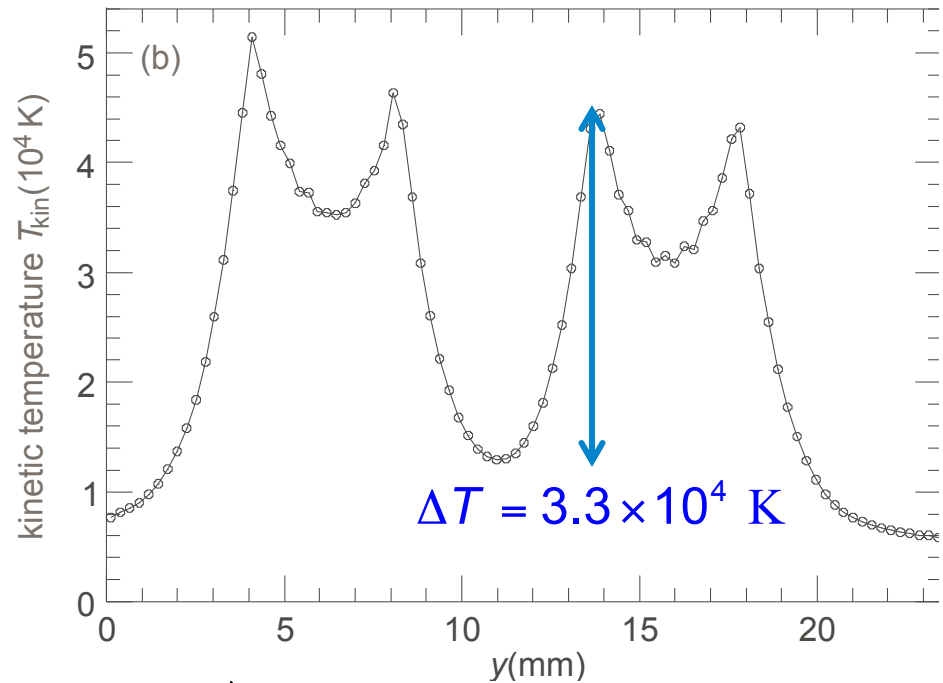
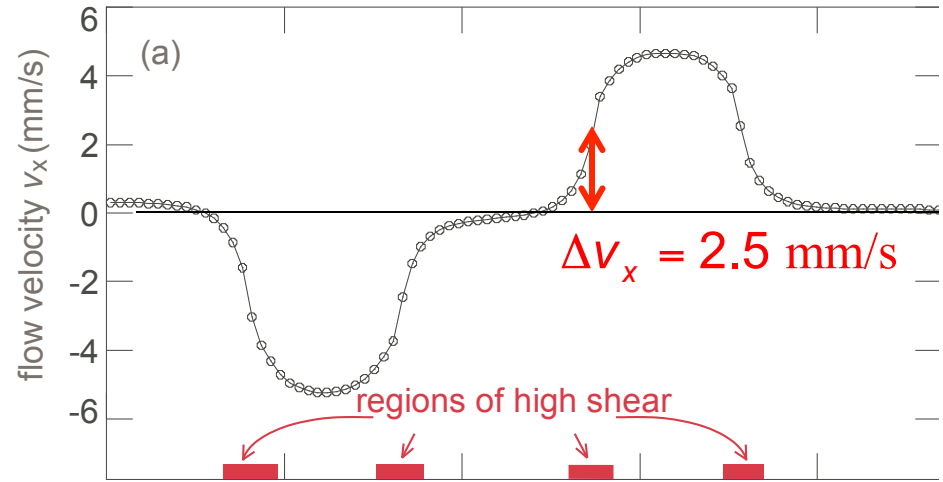
} Material parameters

Calculate the Brinkmann number

Measure the flow parameters:

$$\Delta v_x$$

$$\Delta T$$



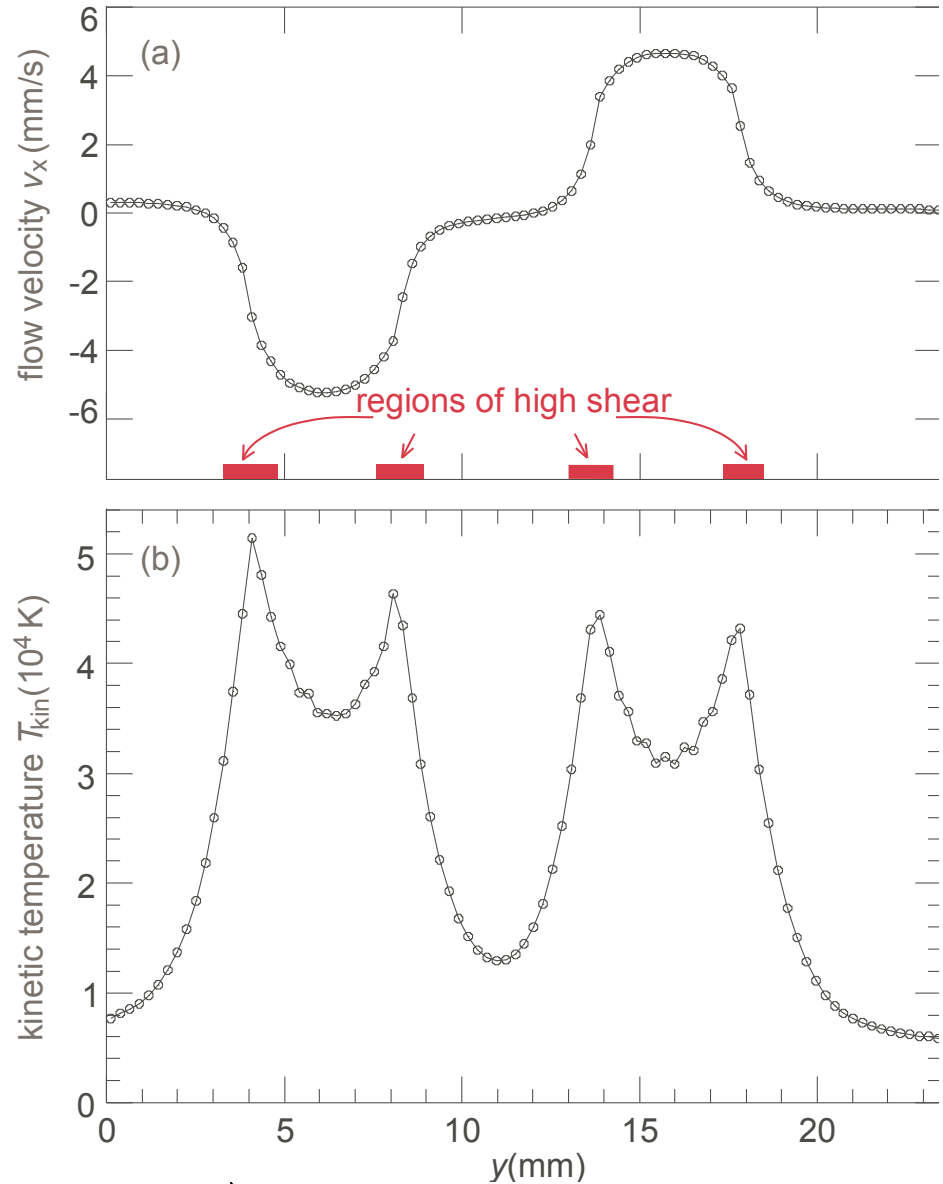
Calculate the Brinkmann number

Measure the material properties:

η

κ

We do this by fitting the profiles to the hydrodynamic equations.



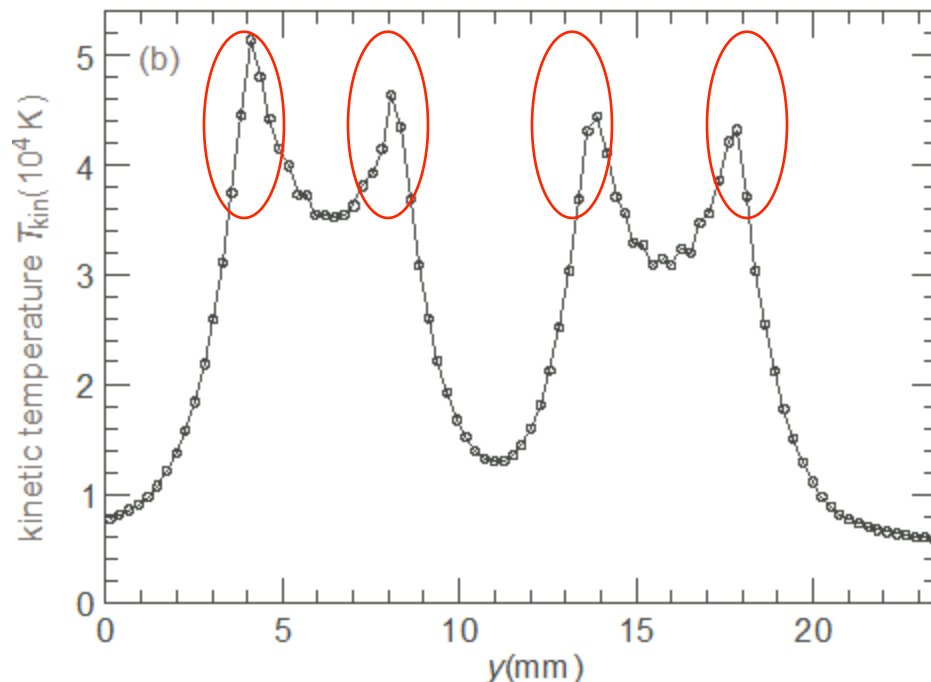
Calculate the Brinkmann number

We find the Brinkmann number

$$\text{Br} \equiv \frac{\eta}{\kappa} \frac{\Delta v_x^2}{\Delta T} \approx 0.5$$

Since $\text{Br} \sim \text{unity}$, this result confirms the conclusion:

We have observed spatially-localized viscous heating.



Our temperature peaks are the elusive “hot spots” of viscous heating.

**DUSTY
PLASMAS**

Observation of Temperature Peaks due to Strong Viscous Heating in a Dusty Plasma Flow

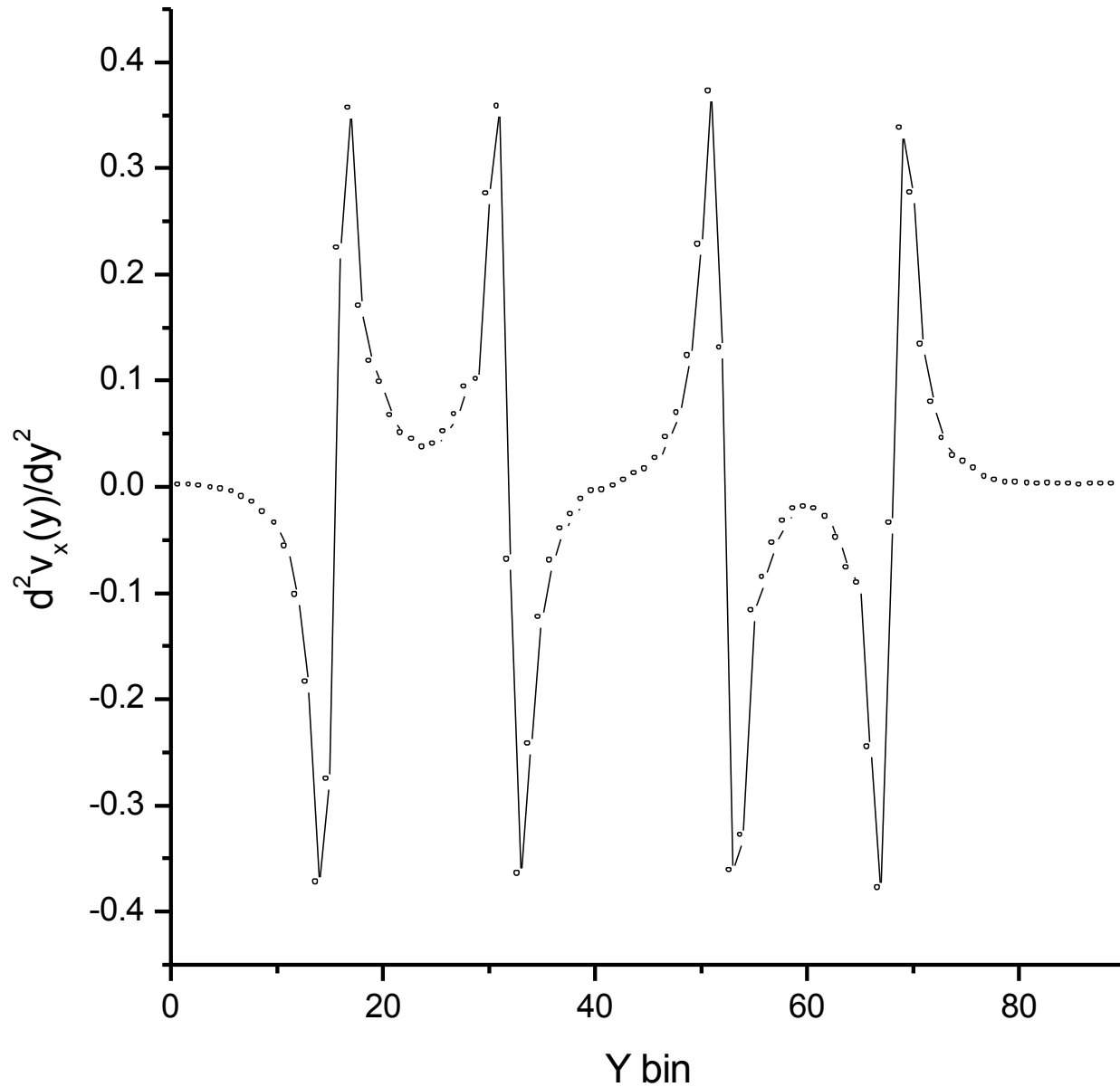
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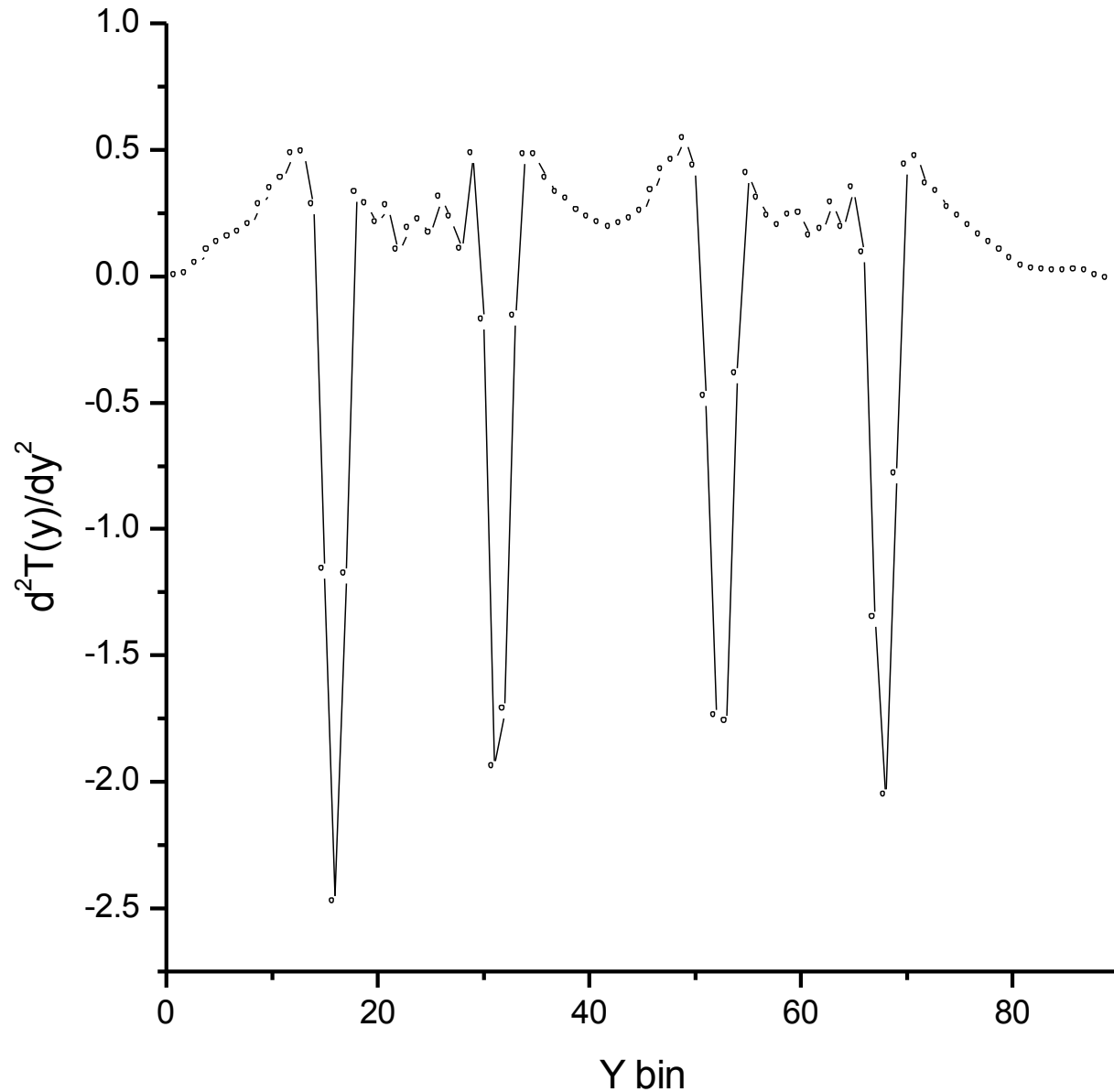
(Received 20 August 2012; published 31 October 2012)

Profound temperature peaks are observed in regions of high velocity shear in a 2D dusty plasma experiment with laser-driven flow. These are attributed to viscous heating, which occurs due to collisional scattering in a shear flow. Using measurements of viscosity, thermal conductivity, and spatial profiles of flow velocity and temperature, we determine three dimensionless numbers: Brinkman, $Br = 0.5$; Prandtl, $Pr = 0.09$; and Eckert, $Ec = 5.7$. The large value of Br indicates significant viscous heating that is consistent with the observed temperature peaks.

Second derivative of the flow velocity



Second derivative of the kinetic temperature



Temperature dependent thermal conductivity $\kappa(T)$

All transport coefficients are temperature dependent, for example κ

$$\frac{\eta}{2\rho} \left(\frac{\partial v_x}{\partial y} \right)^2 + (1/\rho) \frac{\partial}{\partial y} \left(\kappa \frac{\partial T}{\partial y} \right) - \nu \bar{v}^2 = 0$$



$$(\eta/2\rho) (\partial v_x / \partial y)^2 + (\kappa/\rho) \partial^2 T / \partial^2 y + (1/\rho) \frac{\partial T}{\partial y} \frac{\partial \kappa}{\partial y} - \nu \bar{v}^2 = 0$$



Temperature variation is not extreme, so we can assume $\kappa = \kappa_0 + \alpha T$

$$(\eta/2\rho) (\partial v_x / \partial y)^2 + [(\kappa_0 + \alpha T)/\rho] \partial^2 T / \partial^2 y + \alpha (1/\rho) \left(\frac{\partial T}{\partial y} \right)^2 - \nu \bar{v}^2 = 0$$

Temperature dependent thermal conductivity $\kappa(T)$

Minimizing the residual of the energy equation in no laser region

$$\text{Residual}(\kappa) = (\eta/2\rho)(\partial v_x/\partial y)^2 + [(\kappa_0 + \alpha T)/\rho]\partial^2 T/\partial^2 y + \alpha(1/\rho)\left(\frac{\partial T}{\partial y}\right)^2 - \nu v^2$$

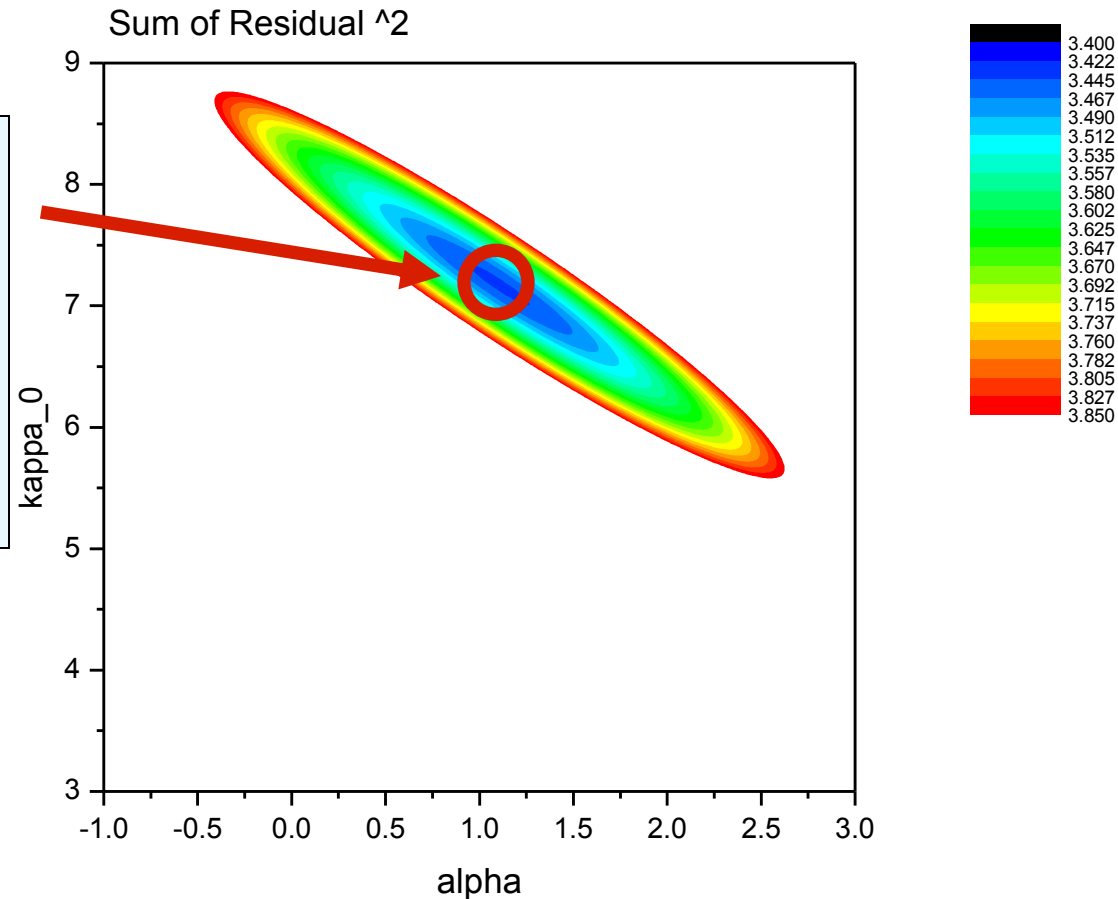
For the region between flows:

$$\frac{\kappa(T)}{\rho} = (7.17 + 1.12v_{thermal\ y}^2) \text{ mm}^2/\text{s}$$

$$v_{thermal\ y}^2 \in [0.42, 0.84]$$

$$\frac{\kappa(T)}{\rho} \in [7.64, 8.11]$$

$$\frac{\kappa}{\rho} = 8.3 \text{ mm}^2/\text{s}$$



Transport coefficients using previous methods

	Our method of minimizing residuals	Previous methods <i>Nosenko and Goree, PRL (2004)</i> <i>Nosenko et al., PRL (2008)</i>
η/ρ		
κ/ρ		
$\kappa(T)/\rho$		

The transport coefficients using our method are consistent with those using different methods.

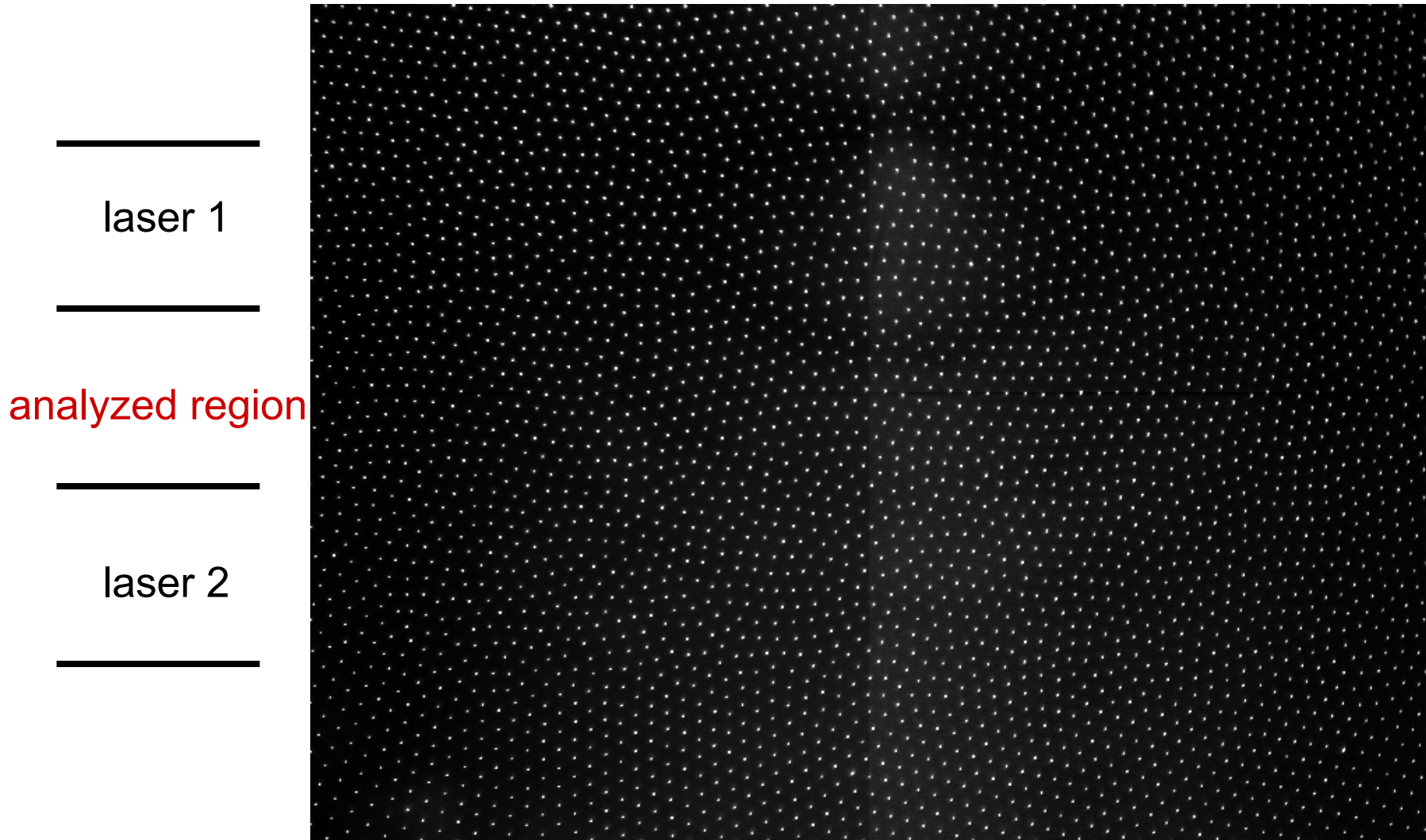
Validity of transport coefficients in 2D systems

Some theorists argue that transport coefficients in 2D system does not exist, due to **non-converging** integrals of the Green-Kubo relation for **uniform** system.

For **non-uniform** systems with a gradient, the analogous test would be to determine whether transport coefficients is **independent** of the scale length.

But, our experiment cannot give a clear answer to this question.

Movie of the laser-driven flow in dusty plasma

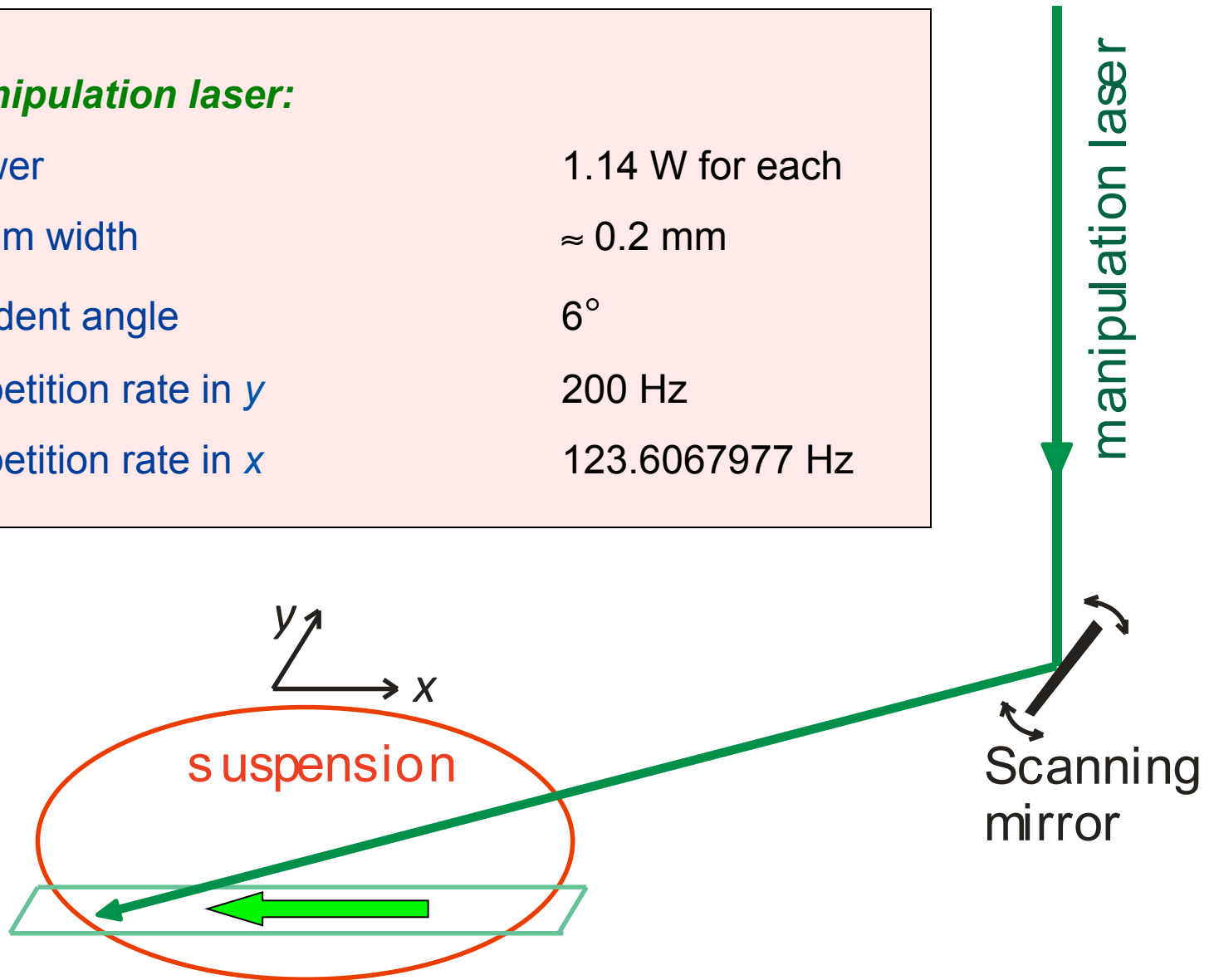


Parameters for laser manipulation

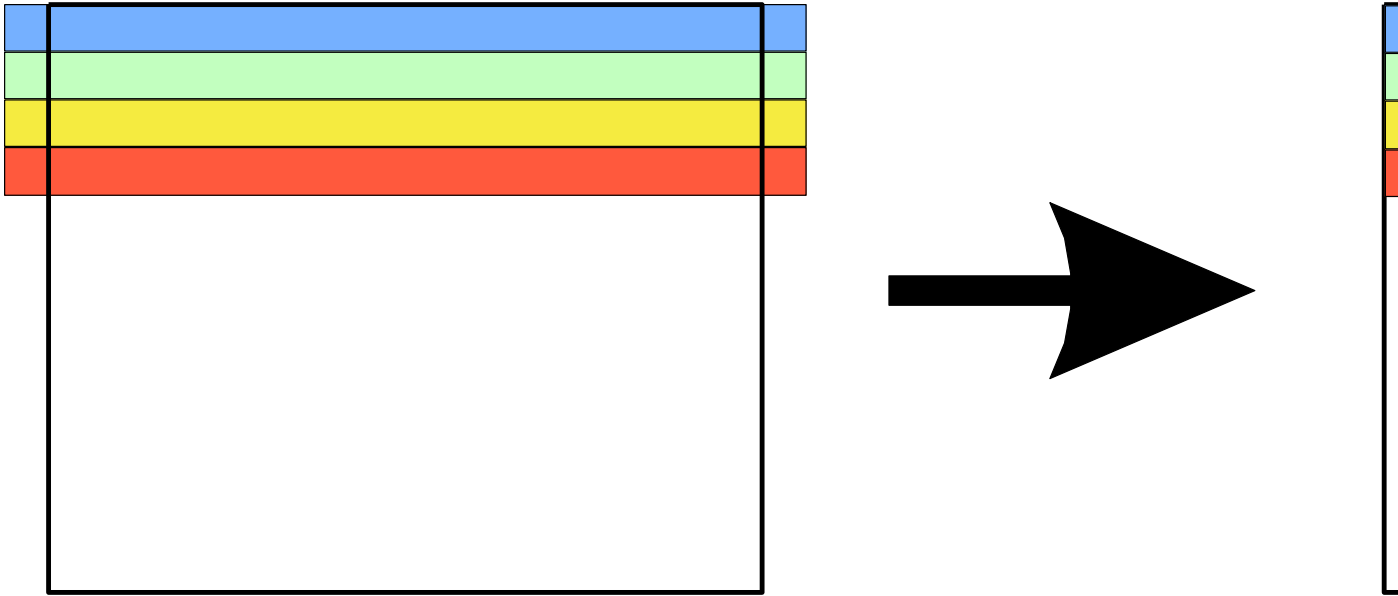
Manipulation laser:

Power	1.14 W for each
Beam width	≈ 0.2 mm
Incident angle	6°
Repetition rate in y	200 Hz
Repetition rate in x	123.6067977 Hz

Improve



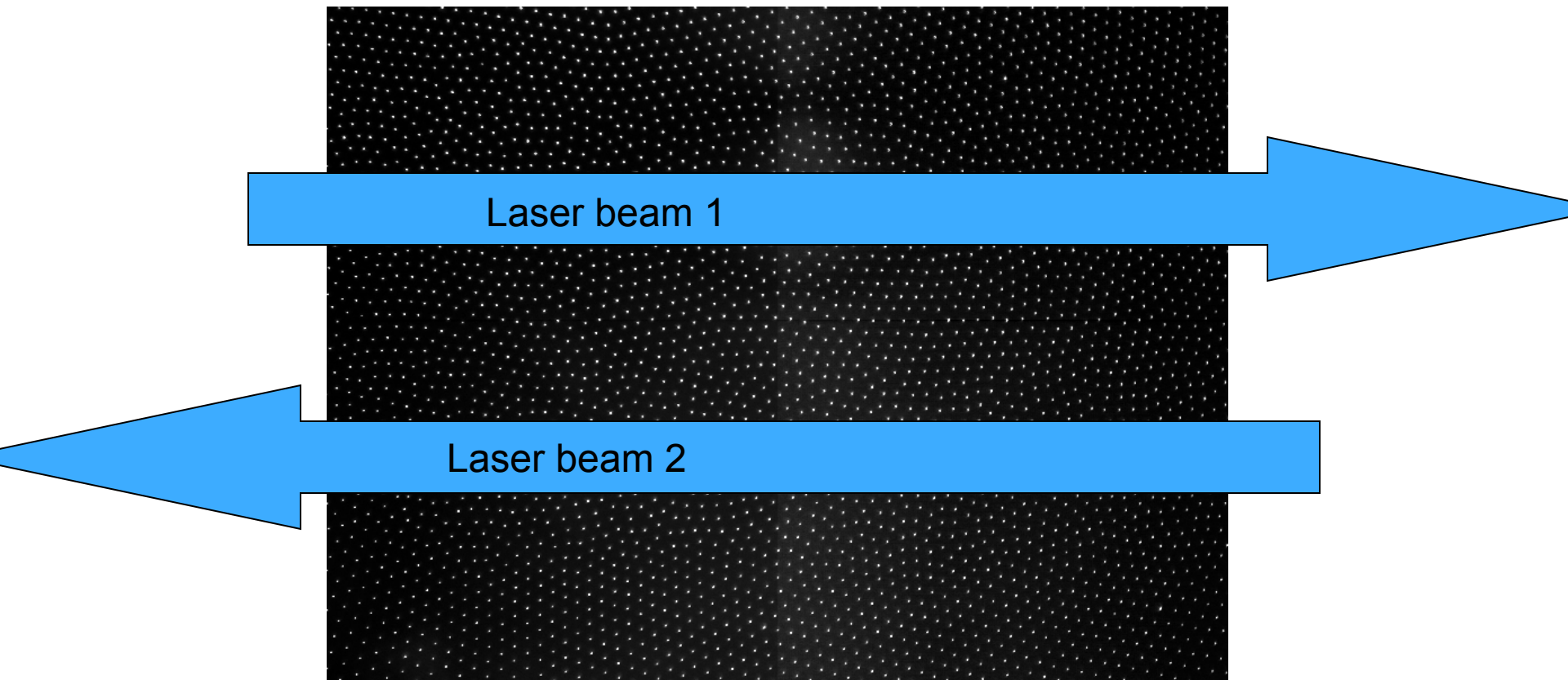
Data analysis: characterize nonuniformity in y



(1) Divide the field of view into 89 bins (of width $\Delta d = r_{ws}$)

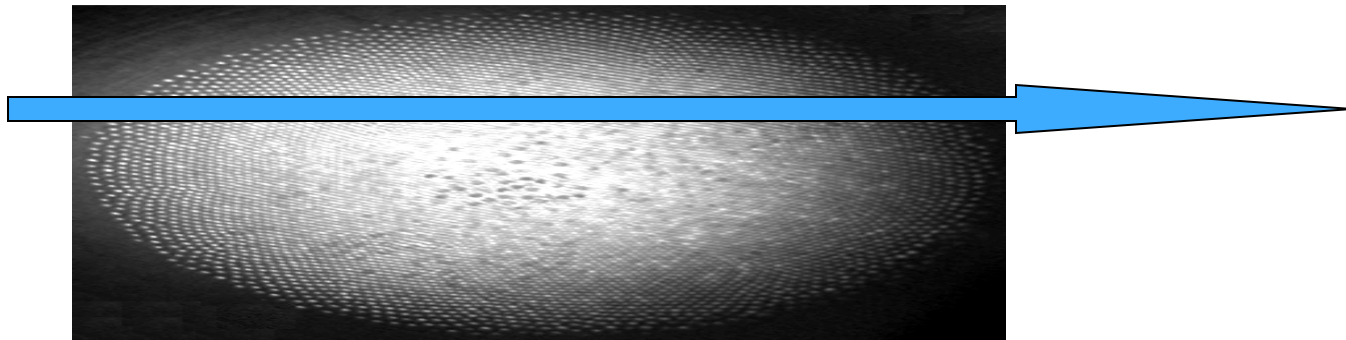
(2) For each frame, **bin** the information (e.g. velocity) of all particles in a stripe

- Each particle contributes to two stripes, according to a “weight”
- weighting factor: Cloud-in-Cell algorithm



Scheme for producing counterpropagating flows

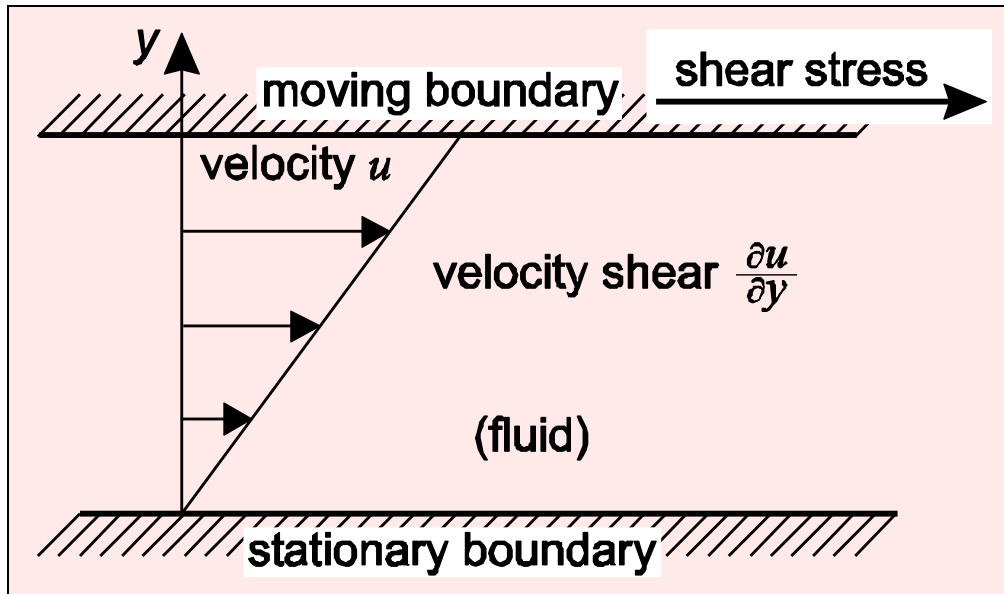
F_{laser} is zero everywhere except within two stripes



What is viscosity?

Viscosity (η)

A measure of how a **fluid** flows under the shear stress.



$$\eta = \text{shear stress} / \frac{\partial u}{\partial y}$$

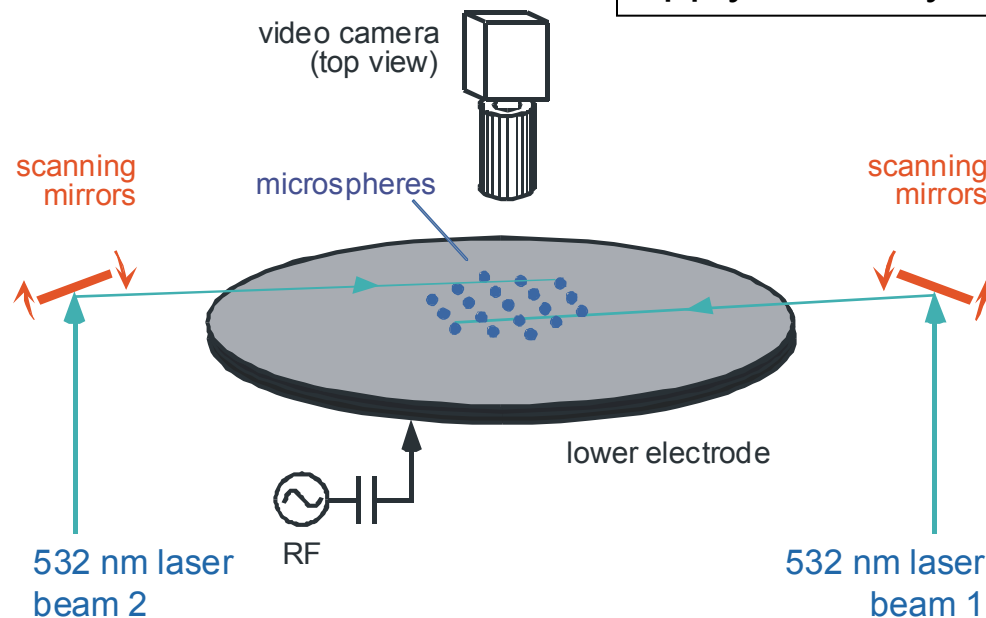
$$\text{kinematic viscosity} = \frac{\eta}{\rho}$$

Measuring η with shear: Setup

Experiment setup

V. Nosenko and J. Goree, PRL (2004)

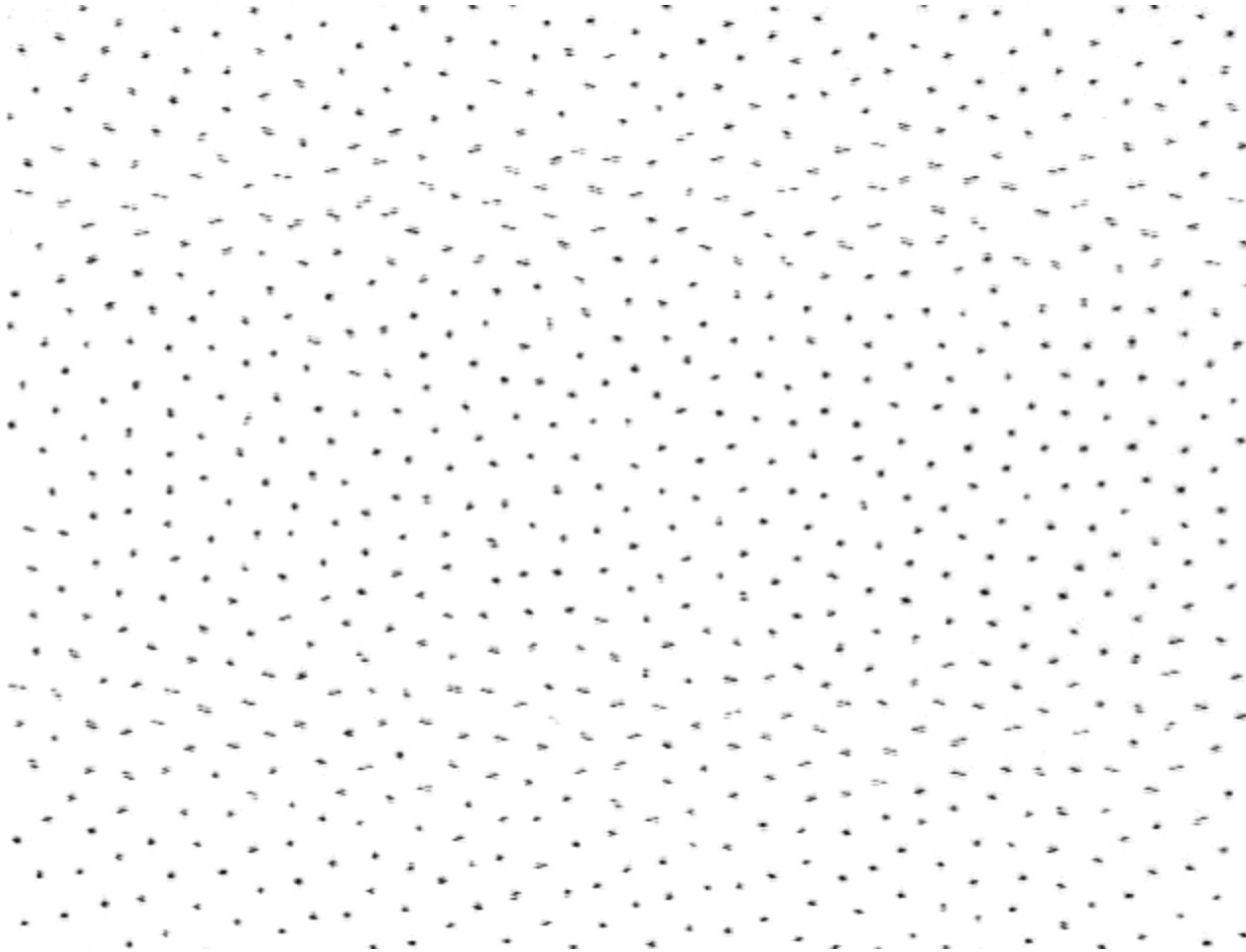
Two laser beams:
apply shear by two counter propagating flows



shear-induced melting

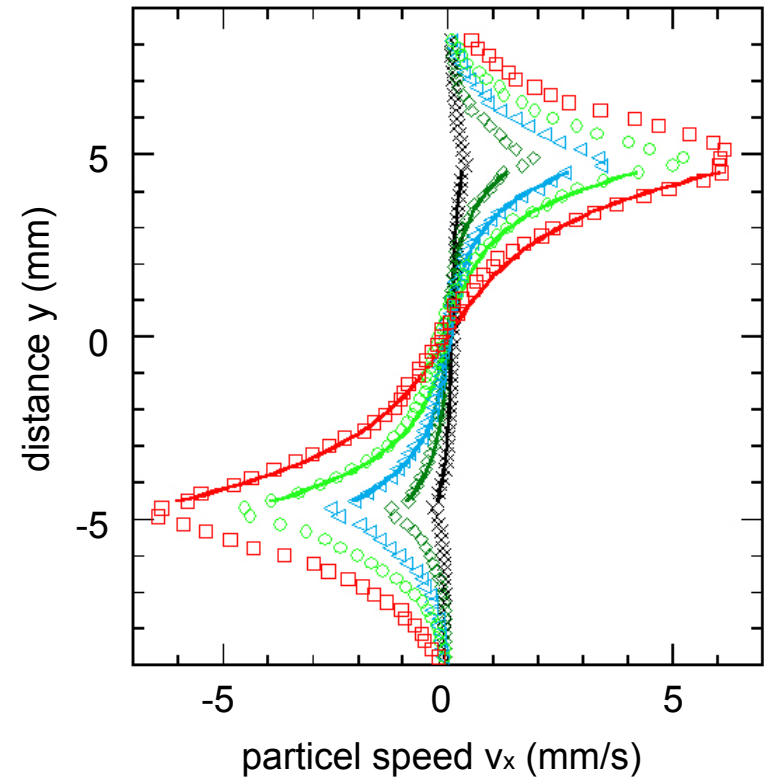
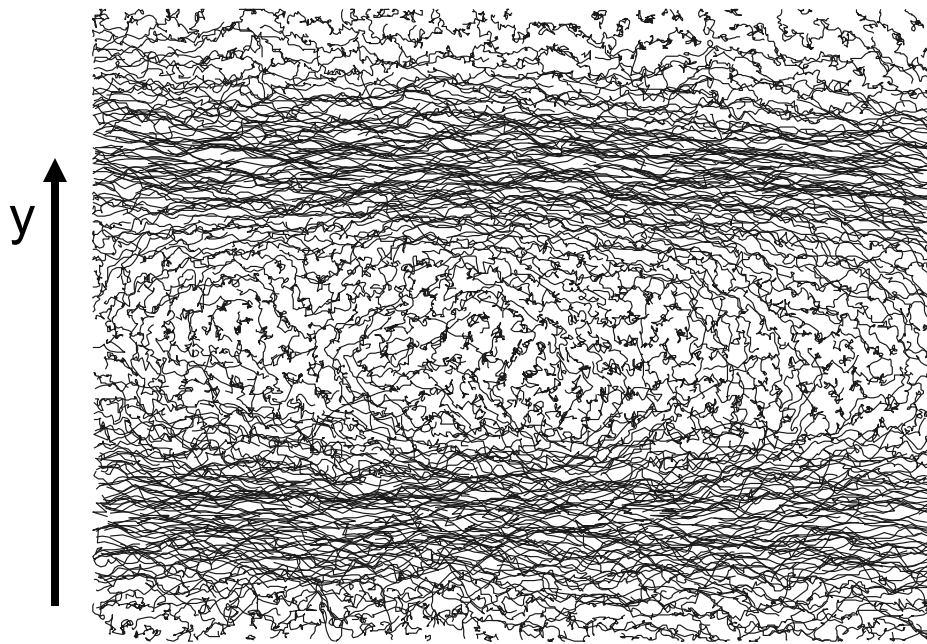
Measuring η with shear: Movie

Movie of suspension with high shear



Measuring η with shear

Particle trajectories



256 frames averaged in steady-state regime

Measuring η with shear: Result

Model the velocity profile to continuum, using Navier-Stokes equation

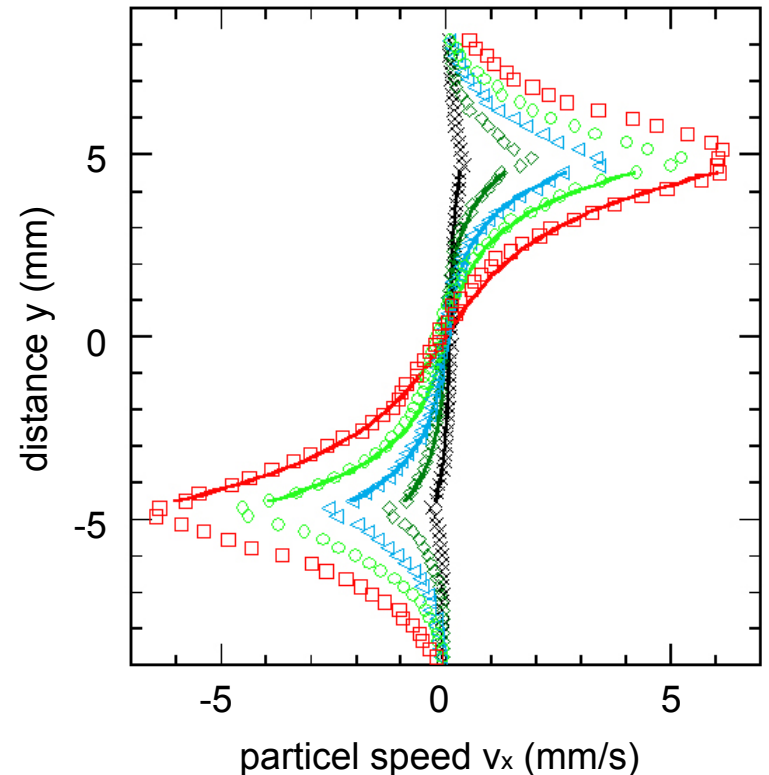
$$\cancel{\frac{\partial \mathbf{v}}{\partial t}} + (\mathbf{v} \cdot \nabla) \mathbf{v} = \cancel{\frac{\nabla p}{\rho}} + \frac{\eta}{\rho} \nabla^2 \mathbf{v} + \left[\frac{\xi}{\rho} + \frac{\eta}{3\rho} \right] \nabla(\nabla \cdot \mathbf{v}) - v_{gas} \mathbf{v}$$

$$\frac{\eta}{\rho} \frac{\partial^2 v_x(y)}{\partial^2 y} - v_{gas} v_x(y) = 0$$

$$v_x(y) = V \sinh(\alpha y) / \sinh(\alpha h)$$

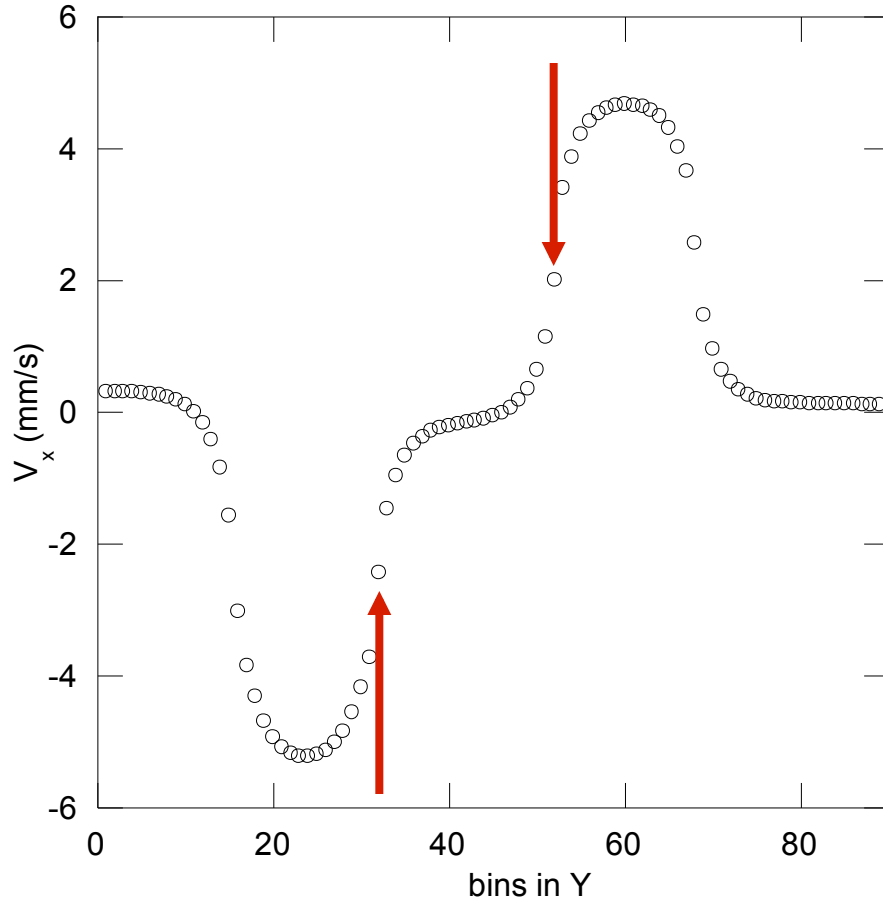
$$\alpha = \sqrt{v_{gas} \rho / \eta}$$

h is the width of between flows



Shear viscosity determination in our experiment

Flow velocity profile $\langle v_x \rangle$



$$v_x(y) = V \sinh(\alpha y) / \sinh(\alpha h)$$

$$\alpha = \sqrt{\nu_{\text{gas}} \rho / \eta}$$

h is the width of between flows

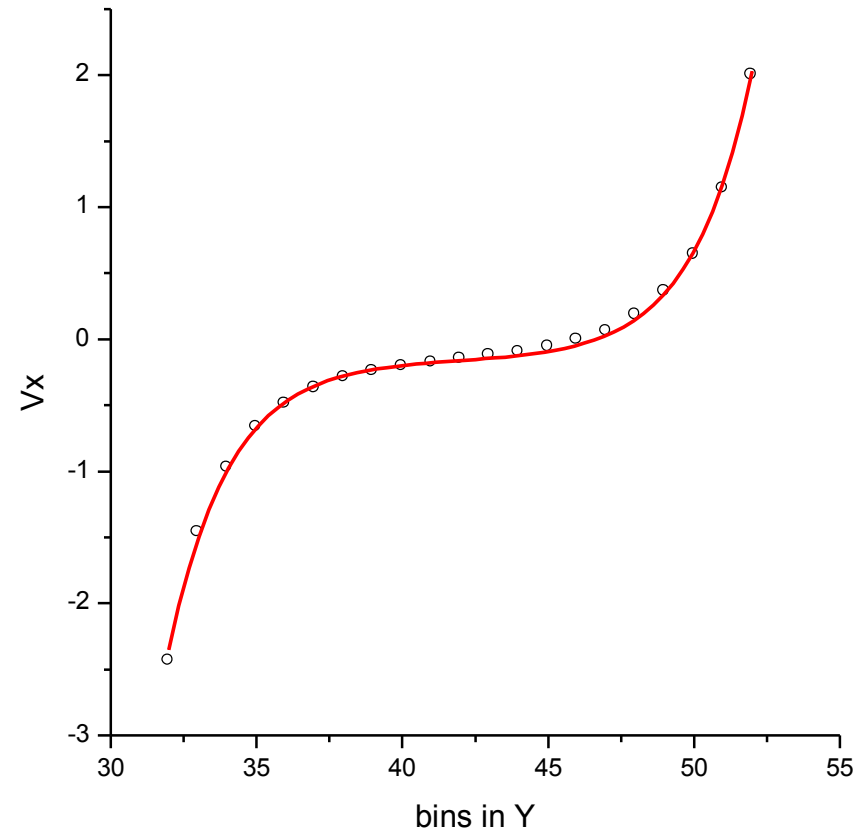
Shear viscosity determination in our experiment

$$v_x(y) = V \sinh(\alpha y) / \sinh(\alpha h)$$

The fitting result of $\alpha = \sqrt{\nu_{\text{gas}} \rho / \eta}$
is not affected by the input value of h

The determined viscosity is

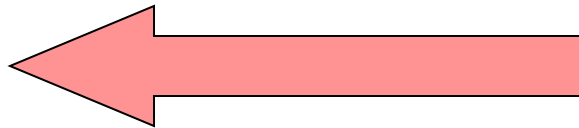
$$\eta / \rho = 0.8 \text{ mm}^2 / \text{s}$$



What is thermal conductivity?

Thermal conductivity (κ)

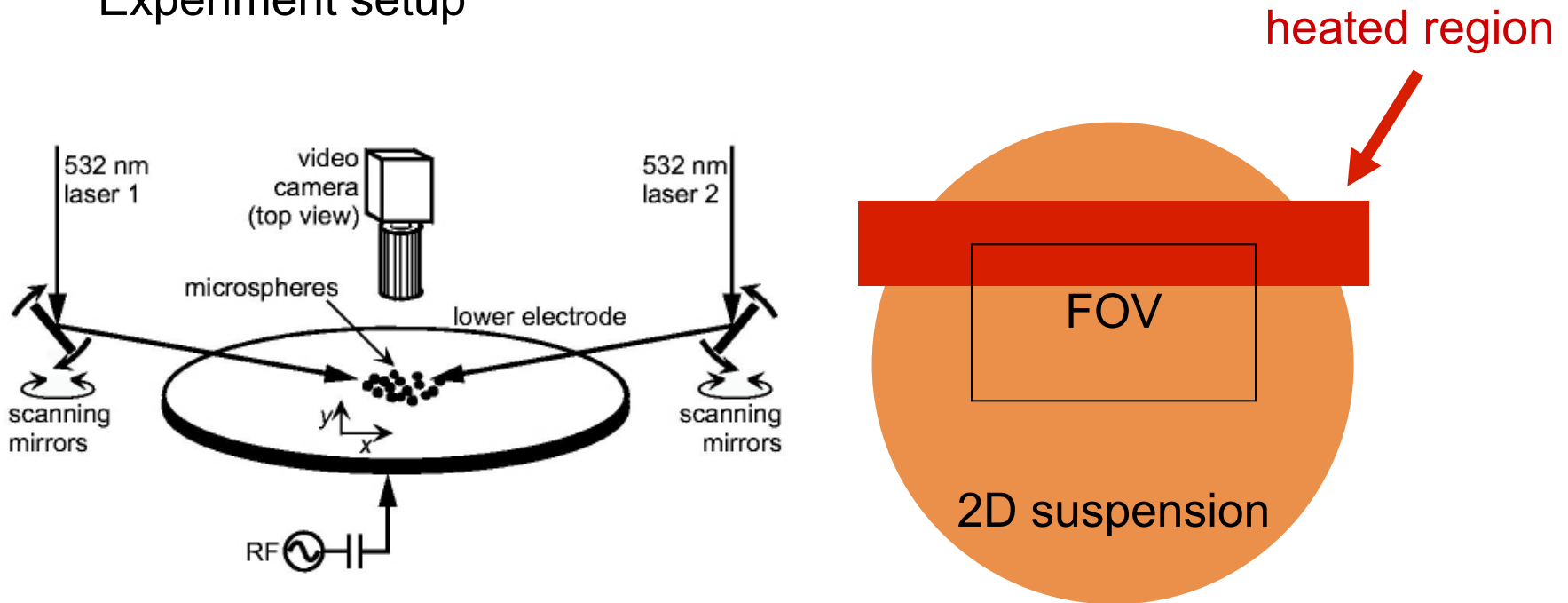
The property of a material's ability to conduct heat.



Heat flux $\dot{q} = \kappa \nabla T$

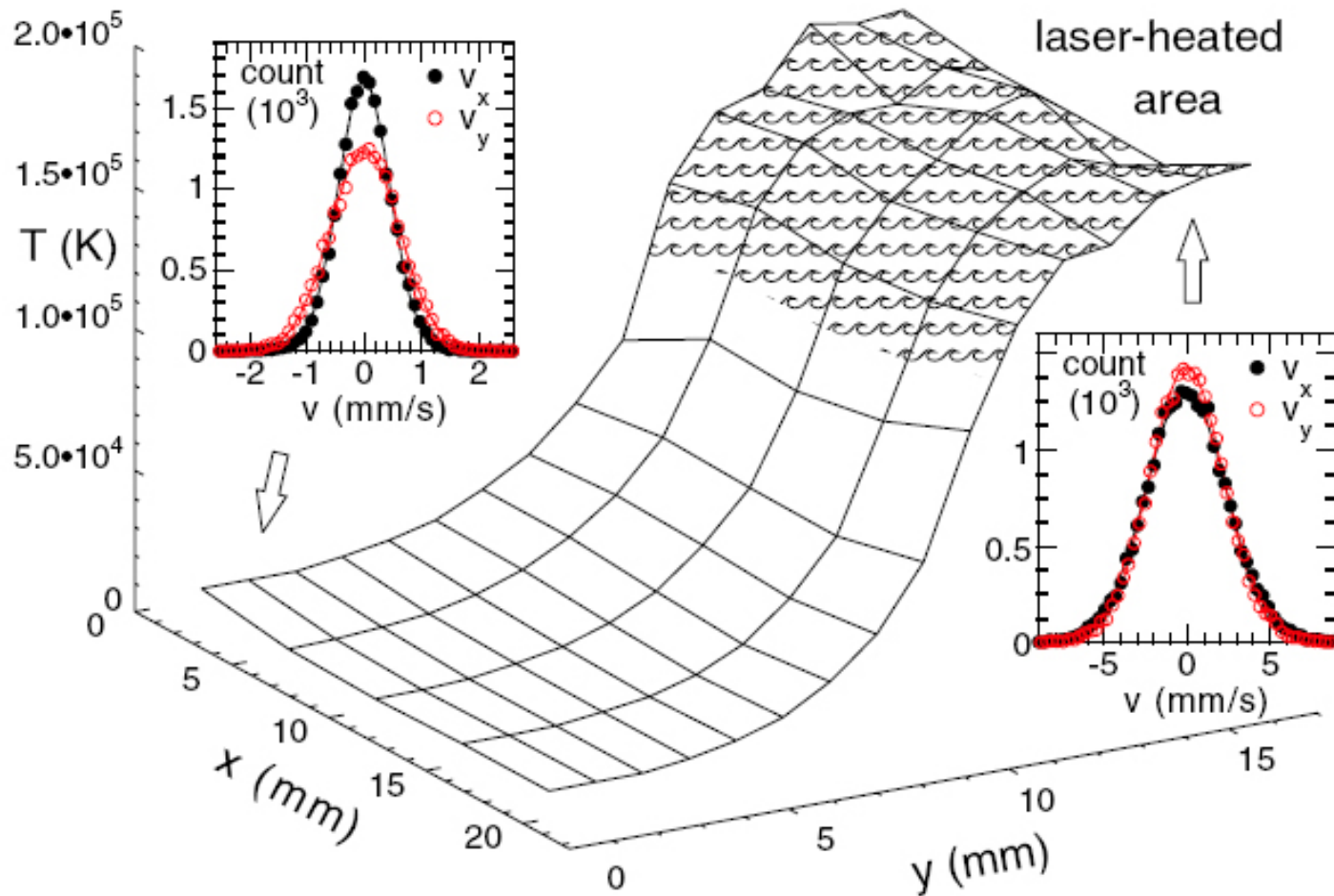
Measuring κ in dusty plasmas: Setup

Experiment setup

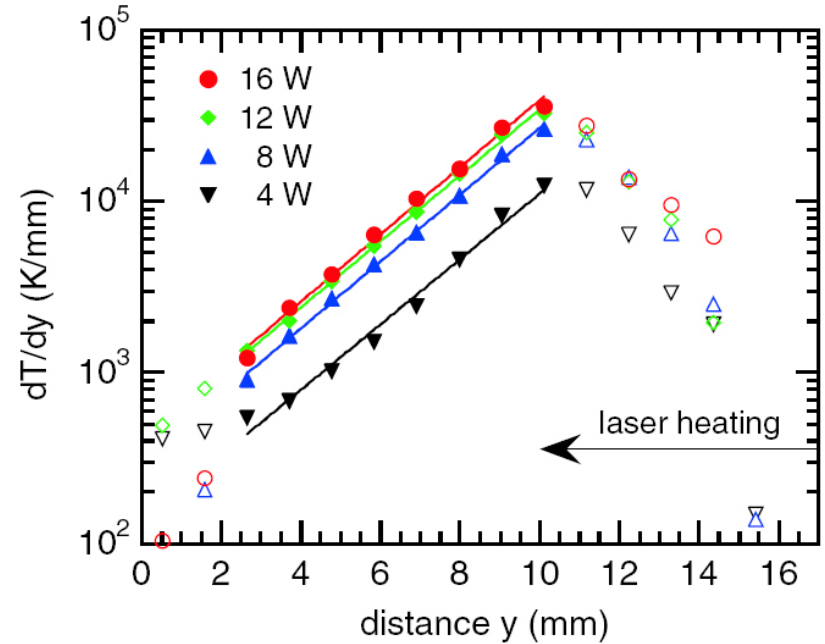
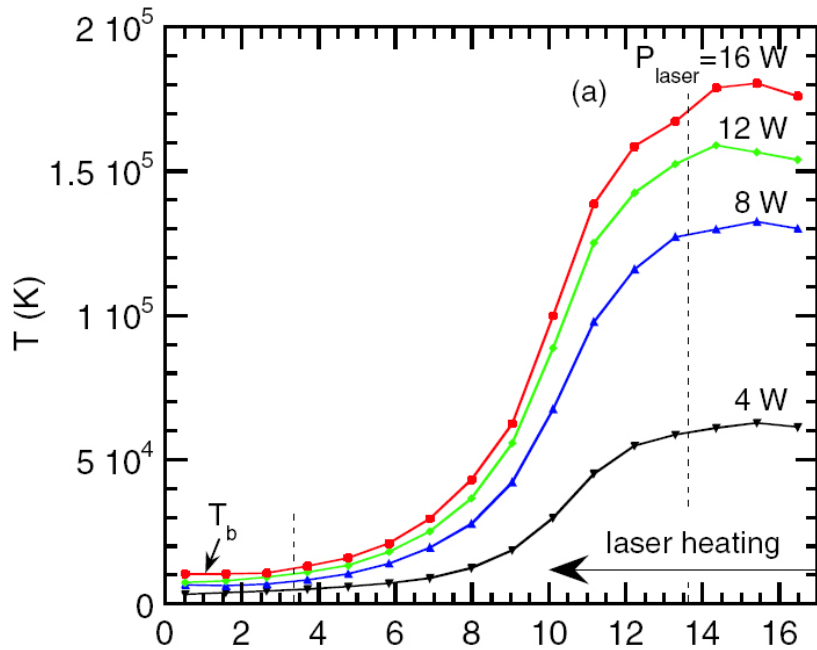


Nosenko et al., PRL (2008)

Measuring κ in dusty plasma



Measuring κ in dusty plasma



Outside laser-heated region, the temperature is about exponential decay.

$$dT/dy \propto \exp(y/L_{\text{heat}})$$

Measuring κ in dusty plasma

Model the dusty plasma suspension to continuum, using fluid equation

$$cn \nabla g \nabla T k_B = \nabla g (\kappa \nabla T) - 2\nu n (T - T_0) k_B + S_{viscous}$$

$$\nabla g (\kappa \nabla T) = 2\nu n (T - T_0) k_B$$

$$dT/dy \propto \exp(y/L_{heat})$$

$$\kappa = 2\nu n L_{heat}^2 k_B$$

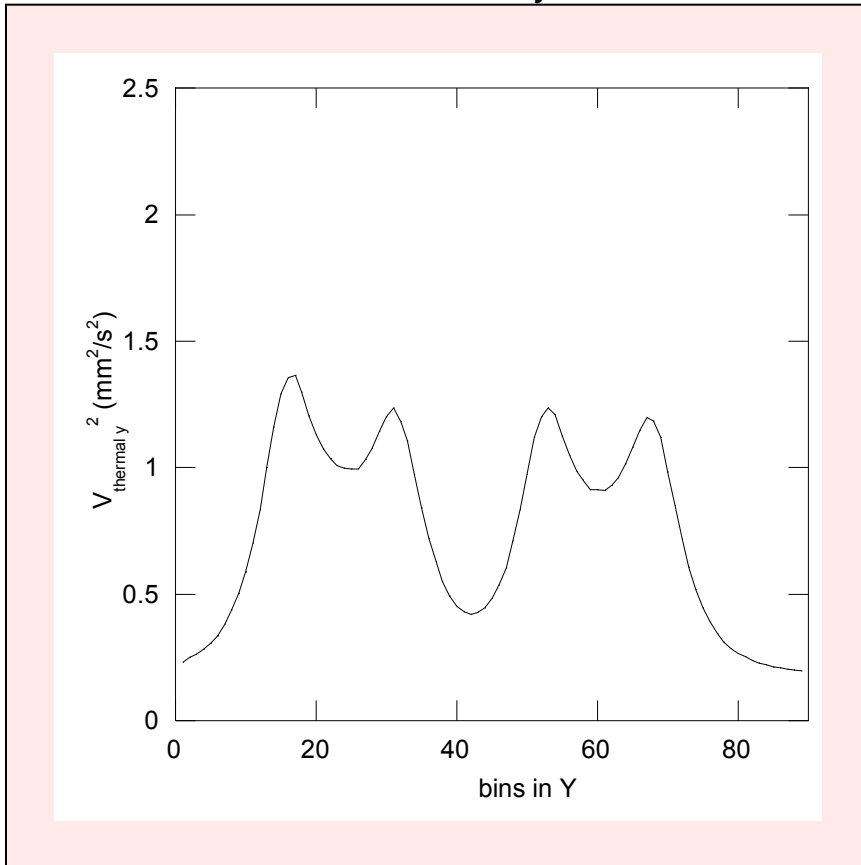
Thermal diffusivity χ is

$$\chi = \kappa / cn = 2\nu L_{heat}^2 k_B / c = 2\nu L_{heat}^2 k_B$$

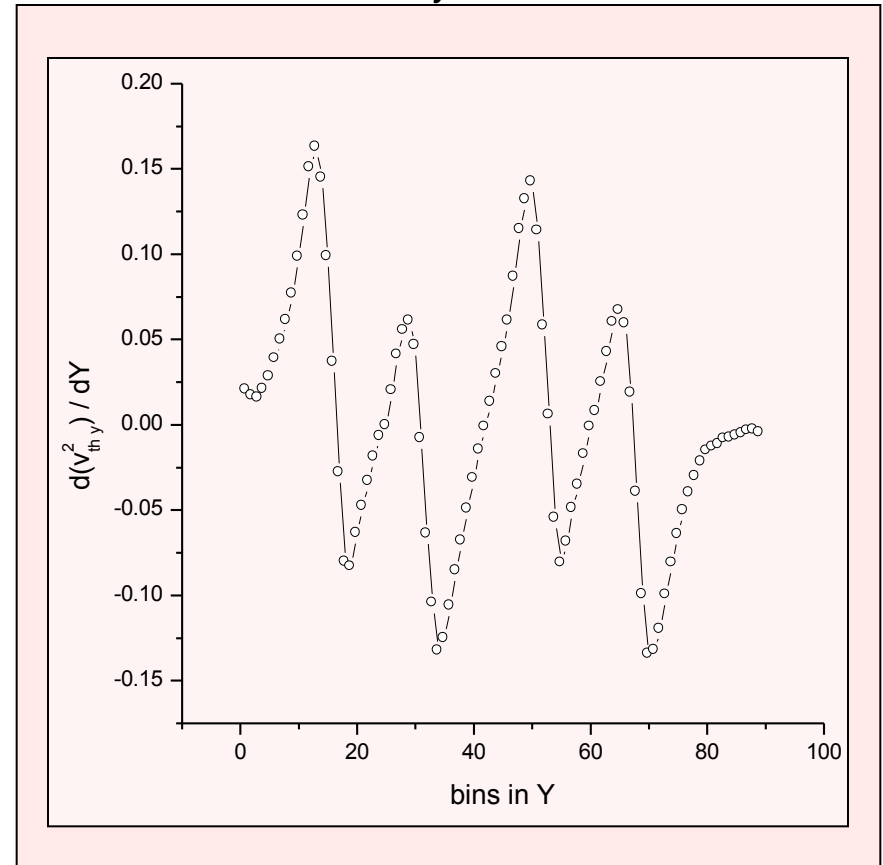
Thermal conductivity determination in our experiment

We use KT_y as the kinetic temperature to determine κ .

$$\langle v_{\text{thermal } y}^2 \rangle$$



$$d \langle v_{\text{thermal } y}^2 \rangle / dY$$



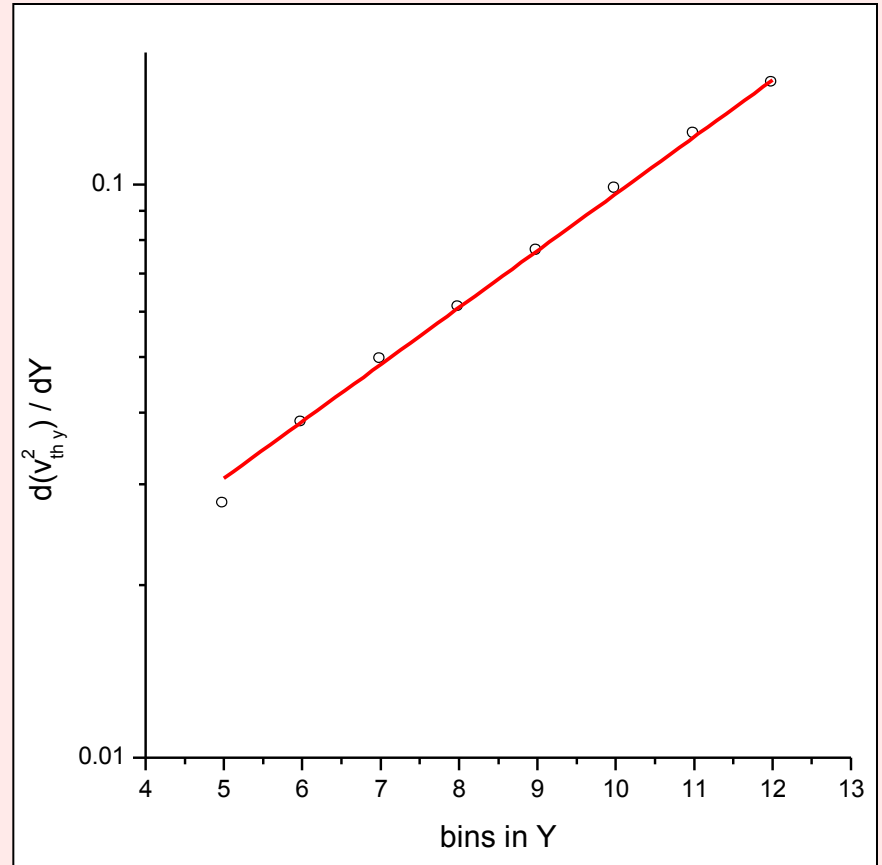
Thermal conductivity determination in our experiment

Thermal diffusivity

$$\chi = \kappa / cn = 2\nu L_{heat}^2$$

Based on our fitting results:

$$L_{heat} = 4.45 \text{ bins}$$



The determined thermal diffusivity is

$$\chi = \kappa / cn = 2\nu L_{heat}^2 = 7.4 \text{ mm}^2 / \text{s}$$

Equation of energy exchange of fluids

For 2D fluids which has a symmetry in the x direction,
the energy equation is:

$$T \frac{DS}{Dt} = \frac{1}{2} \frac{\eta}{\rho} \left(\frac{\partial v_x}{\partial y} \right)^2 + \frac{\kappa}{\rho} \frac{\partial^2}{\partial y^2} (T) \quad \text{energy dissipation per unit mass}$$

Batchelor, An Introduction to Fluid Dynamics (1979)

viscous heat heat conduction

For our dusty plasma, we also need to consider:

- The dissipation due to gas damping
- The energy input due to laser manipulation

Dissipation due to gas damping

Gas drag friction coefficient

$$\nu = F / m_{dust} v_{dust} = 2.7 \text{ s}^{-1}$$

Gas damping force

$$F = \nu m_{dust} v_{dust}$$

Energy dissipation due to gas damping per unit mass

$$P = F v_{dust} / m_{dust} = \nu v_{dust}^2$$

Hydrodynamic Equations

Navier-Stokes equation

momentum

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v}\nabla)\mathbf{v} = -\frac{\nabla p}{\rho} + \frac{1}{\rho} \nabla g(\eta \nabla \mathbf{v}) + \left[\frac{\zeta}{\rho} + \frac{\eta}{3\rho} \right] \nabla(\nabla g \mathbf{v})$$

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v}\nabla)\mathbf{v} = -\frac{\nabla p}{\rho} + \frac{\eta}{\rho} \nabla^2 \mathbf{v} + \left[\frac{\zeta}{\rho} + \frac{\eta}{3\rho} \right] \nabla(\nabla g \mathbf{v}) \quad \text{force per unit mass}$$

energy

$$\frac{DH}{Dt} = \frac{1}{\rho} \frac{Dp}{Dt} + \frac{1}{\rho} \nabla g(\kappa \nabla T) + \frac{1}{\rho} \Phi$$

energy dissipation per unit mass

Batchelor, An Introduction to Fluid Dynamics (1979)

Forces in the momentum equation

Delete?

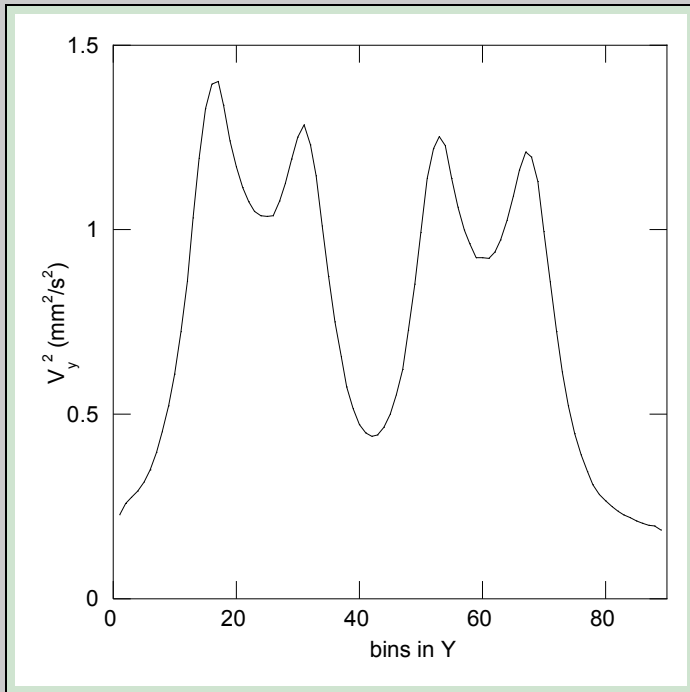
Momentum equation

The main horizontal forces acting on the dust particles:

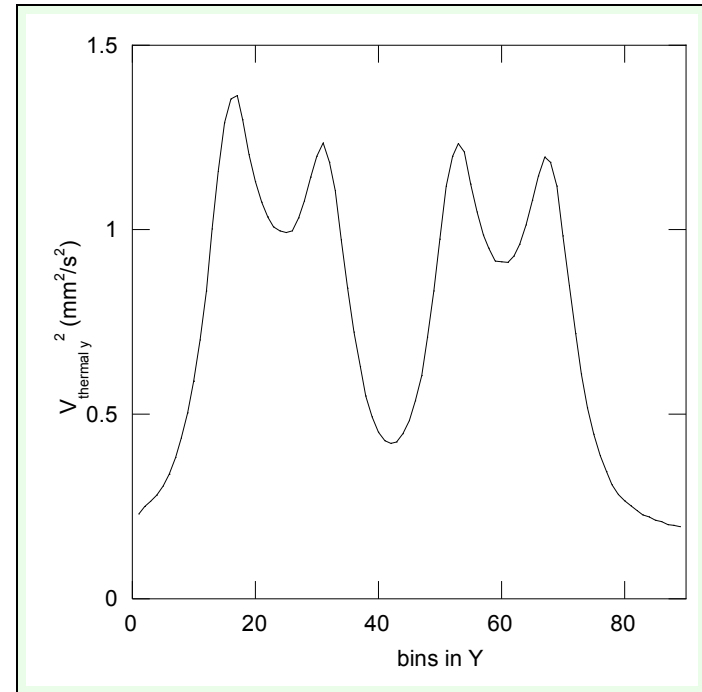
- Inter-particle electric repulsion (Coulomb collisions)
 - Responsible for transport coefficients η kappa
- radiation pressure force from laser manipulation
- gas drag (friction) force

Profile of kinetic energy (contribution due to y-component of particle velocity)

with the contribution of the flow velocity



without the contribution of the flow velocity



$$2k_B T / m_{\text{part}} = \frac{1}{N} \sum_{i=1}^N [v_{\text{part } i} - v_{\text{flow}}(y)]^2$$

$v_{\text{flow}}(y)$ is flow velocity at y , interpolated between grid centers

What is thermal conductivity?

Thermal conductivity (κ)

The property of a material's ability to conduct heat.



$$\text{Heat flux } \dot{q} = \kappa \nabla T$$

What is viscosity?

Viscosity (η)

A measure of how a **fluid** flows under a shear force (shear stress).

$$\eta = \text{shear stress} / \frac{\partial v_x}{\partial y}$$

Example:

Couette flow, apply a stress (force per unit area) to the top plate:

